



The SALEMA Project Journey: main outcomes, challenges and possibilities

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21st March 2024 – SALEMA FINAL EVENT



Summary

- Project introduction and video
- Scrap sorting system
- Development of HPDC SALEMA alloys
- Validation of HPDC SALEMA alloys in Shock Tower
- Alloy development and industrial validation in Hot Stamping
- Alloy development and industrial validation in extrusion
- Validation procedure of new alloys by an OEM



PROJECT GOAL



European Green Deal poses multiple challenges for the automotive industry:

- Need for new, high-performance but lightweight materials
- Decrease the dependencies on imported raw materials while creating a sustainable economy for the future

SALEMA Main objectives:

- To develop a non-CRM dependent aluminium ecosystem, by exploring 2 different approaches:
 - By **substituting primary CRMs with alternative** and commonly available elements
 - By obtaining the **CRMs elements from domestic scrap**, significantly increasing the amount of recycled material

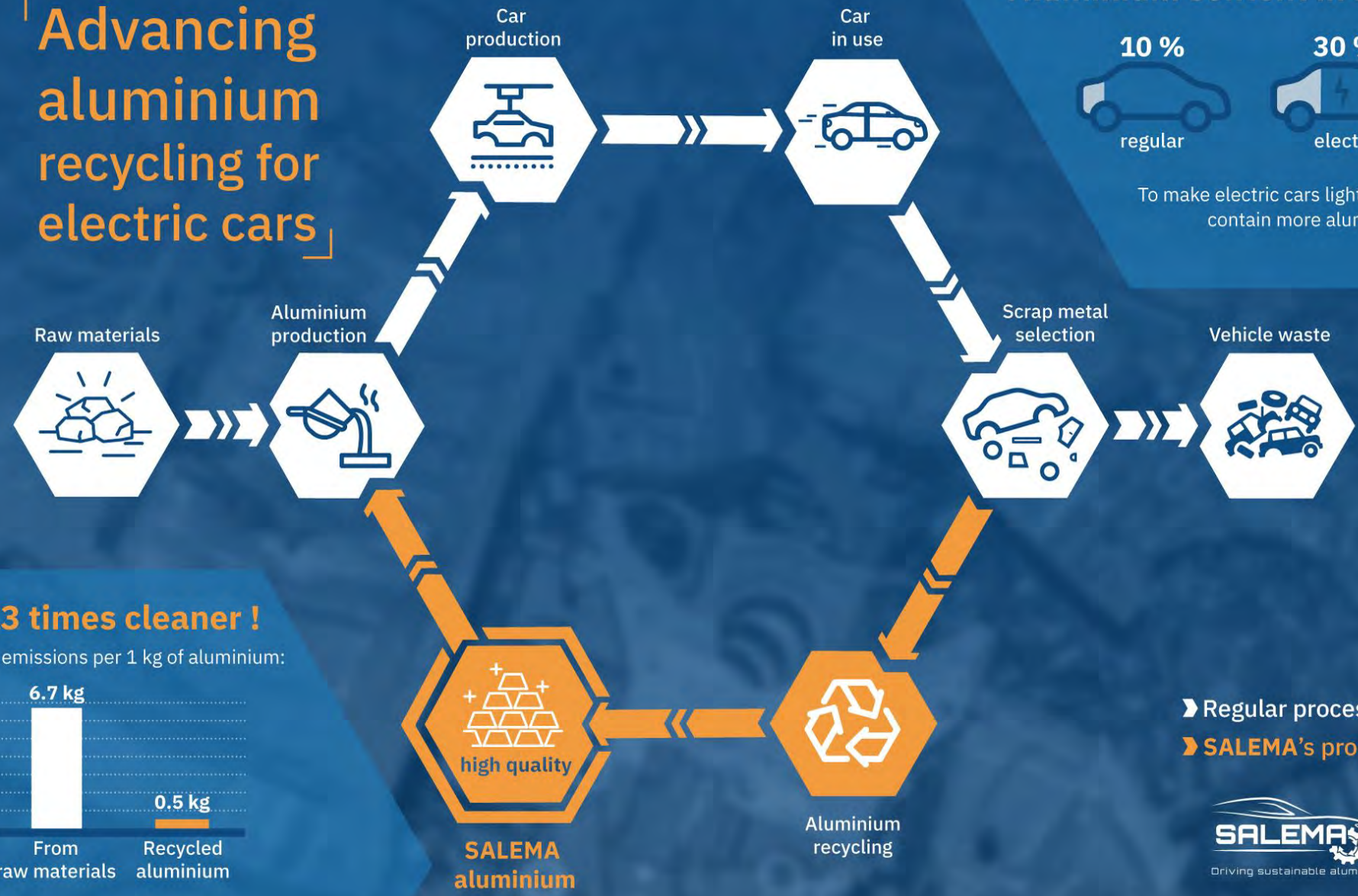


Advancing aluminium recycling for electric cars

Aluminium content in a car



To make electric cars lighter they contain more aluminium.



13 times cleaner !

CO₂ emissions per 1 kg of aluminium:



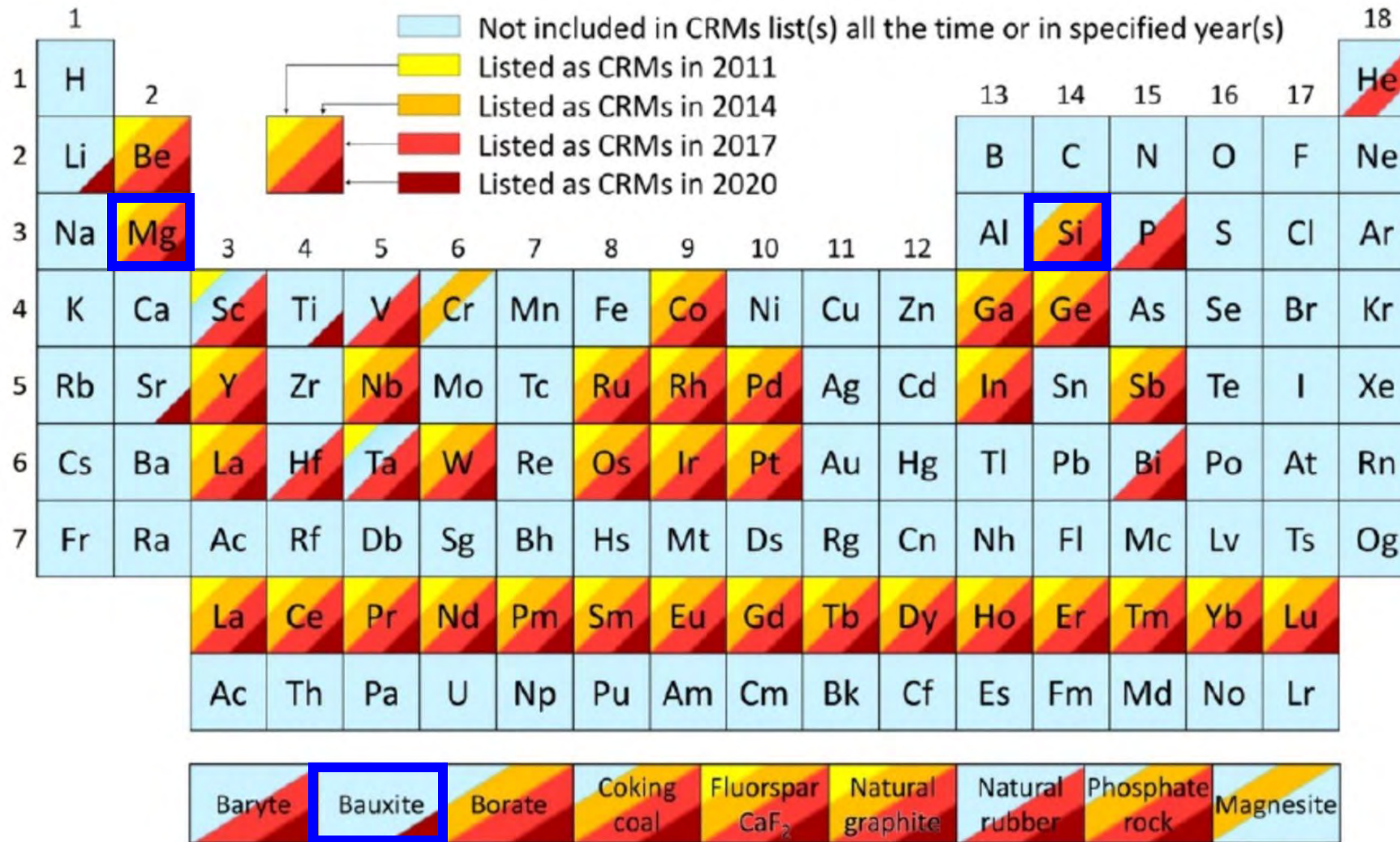
- ▶ Regular process
- ▶ SALEMA's process



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.



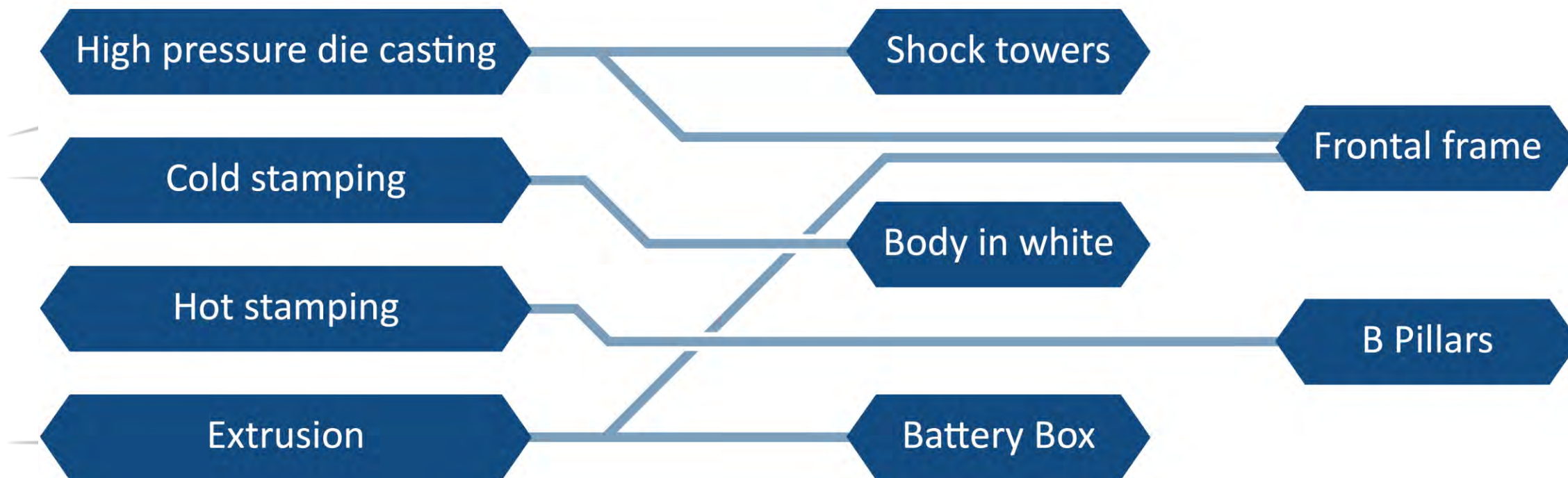
Critical Raw Materials (CRMs) for the EU



- Aluminium is a lightweight and cost-effective material
- Production of Aluminium and its alloys requires bauxite and other Critical Raw Materials (CRM), such as Si and Mg

4 PILOTS

5 DEMONSTRATORS



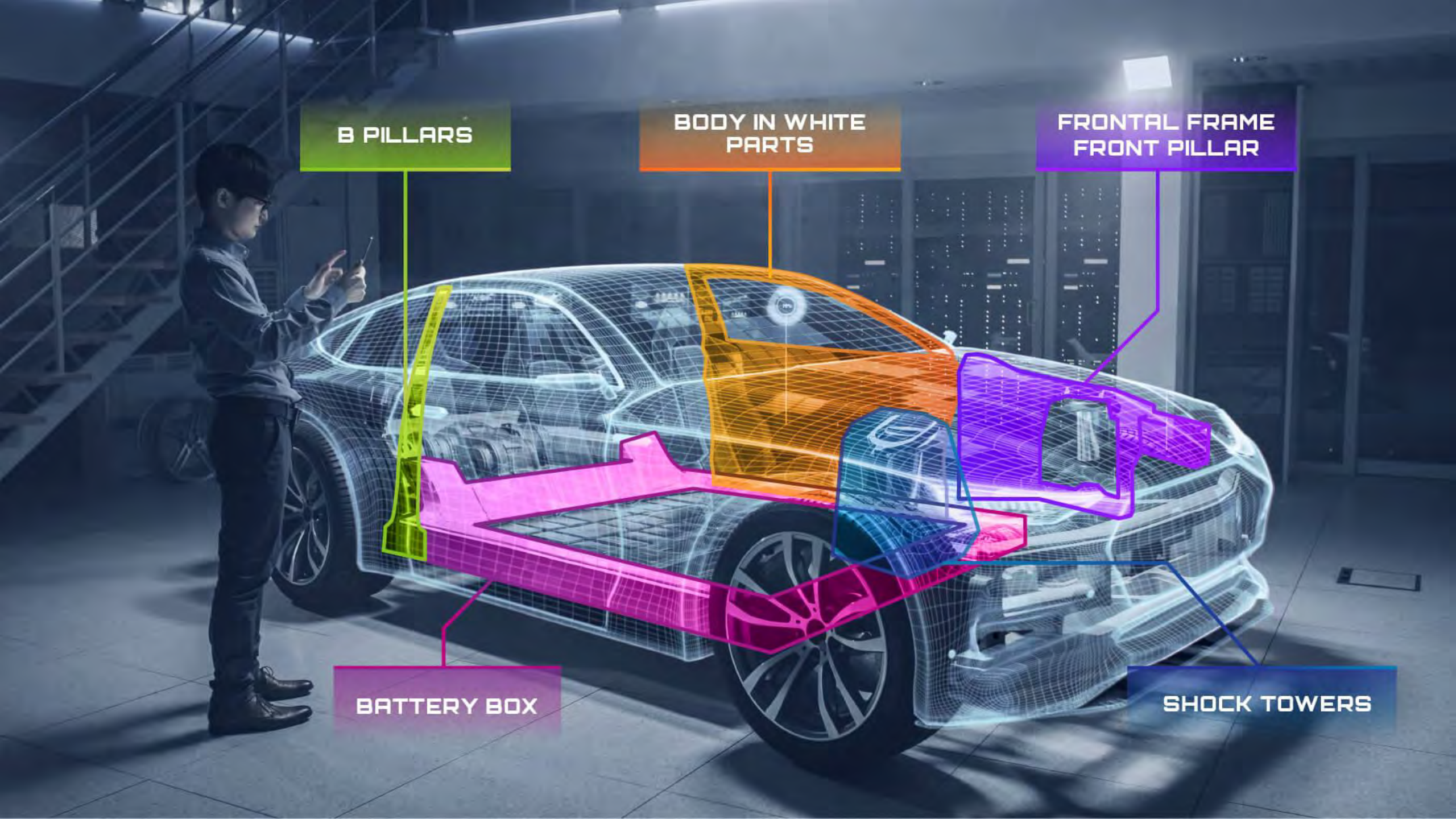
B PILLARS

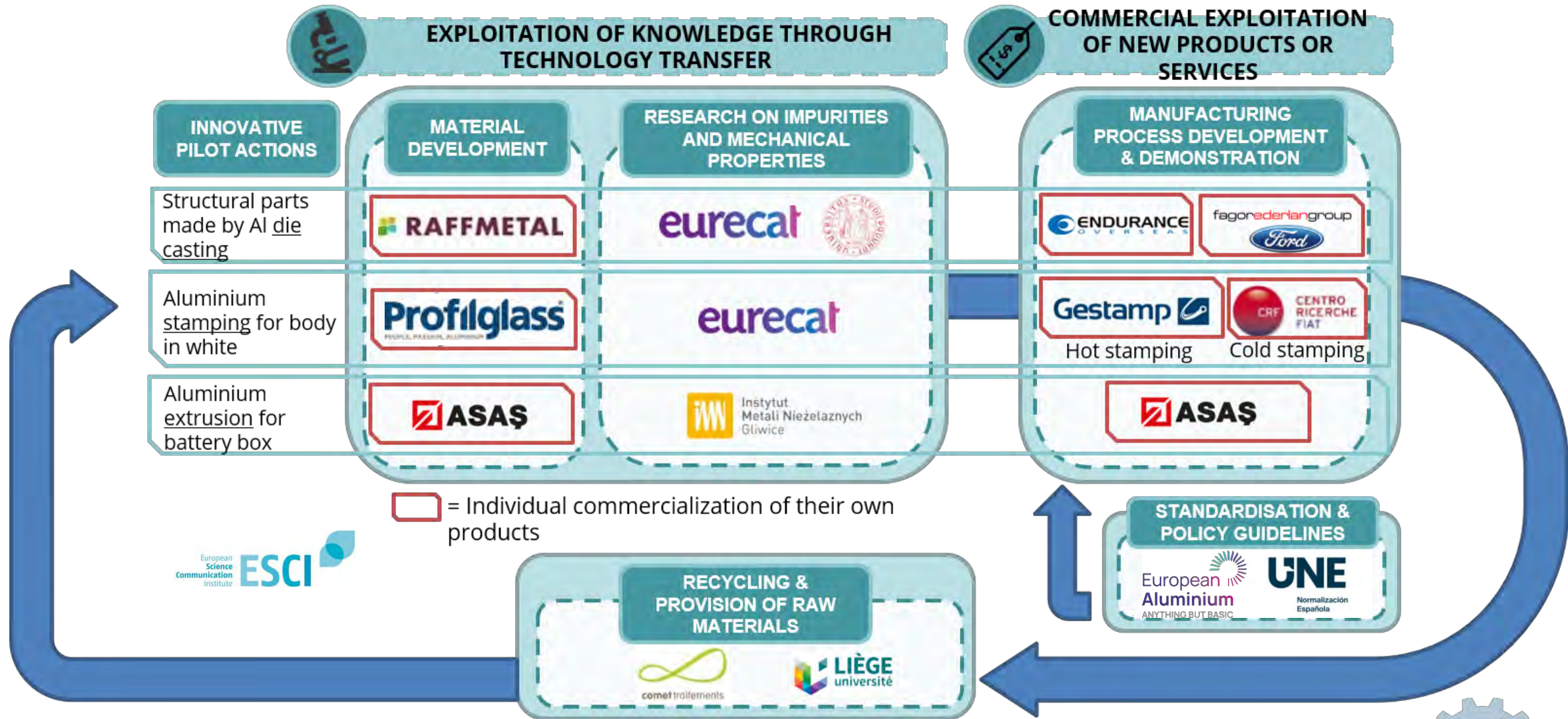
BODY IN WHITE PARTS

**FRONTAL FRAME
FRONT PILLAR**

BATTERY BOX

SHOCK TOWERS





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- FINAL VIDEO



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SCRAP SORTING SYSTEM



Objectives

- Adapt PICKIT sorting prototype to **separate post-consumer scraps** based on their alloying elements with LIBS.

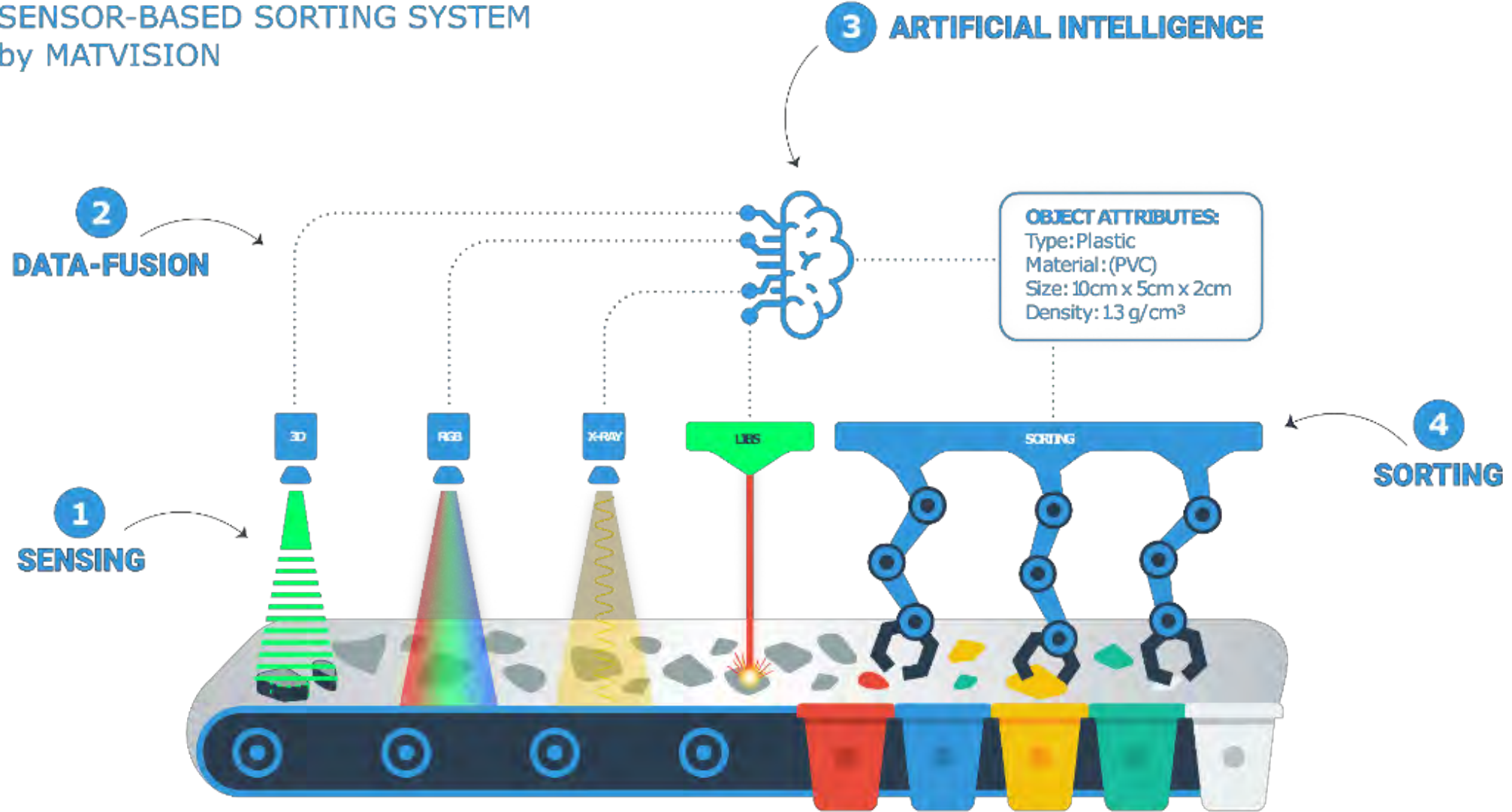
Results

- Successfully produced **high-quality lots of 1xxx, 2xxx, 3xxx, 5xxx & 6xxx** for industrial validation with SALEMA's partners



SCRAP SORTING SYSTEM

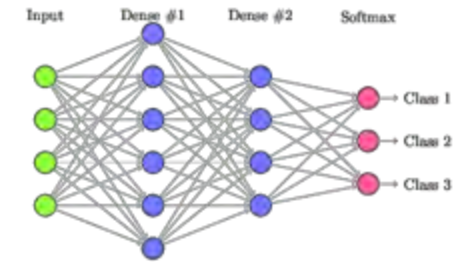
SENSOR-BASED SORTING SYSTEM
by MATVISION



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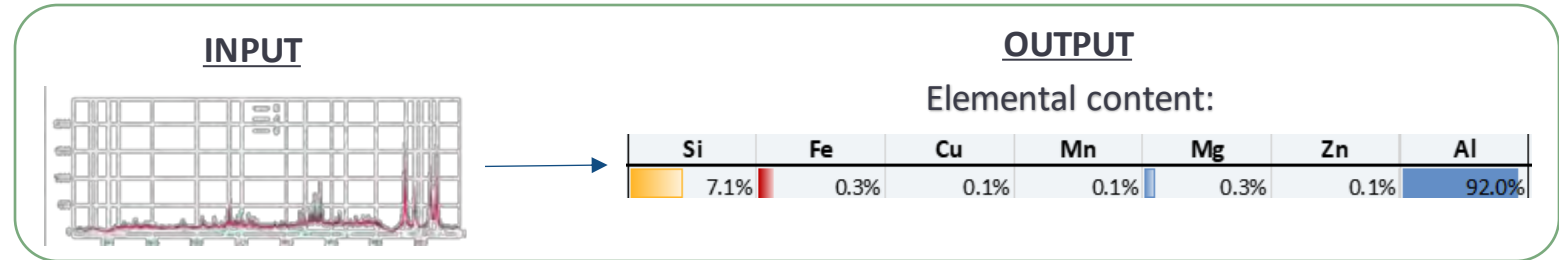


SCRAP SORTING SYSTEM

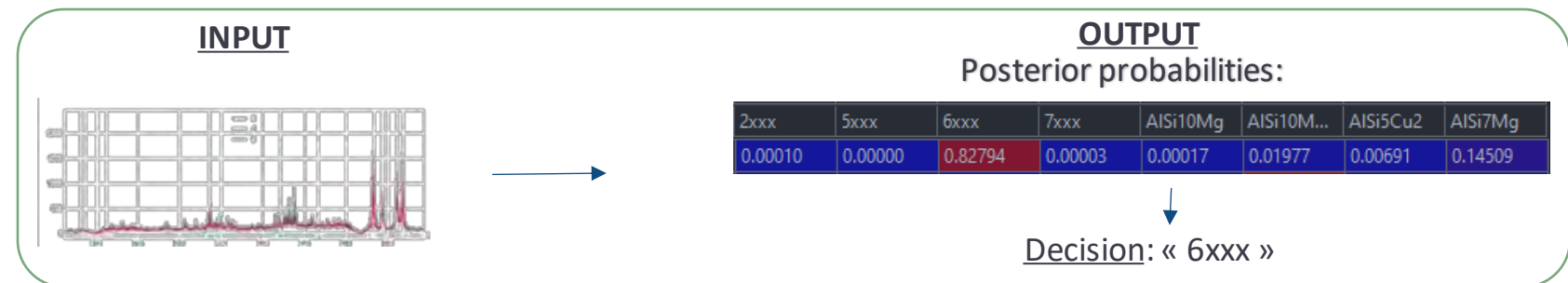


Two complementary approaches:

- Multi-output regression models:
=> Chemical content estimation



- Classification models:
=> Decision for sorting





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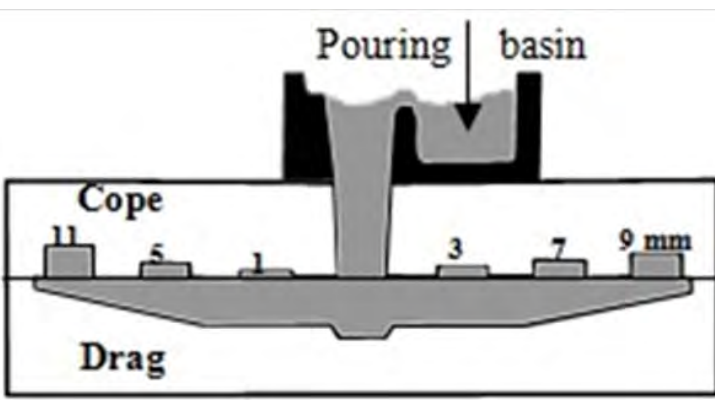


HPDC ALLOY DEVELOPMENT

n=5	%Si	% Fe	%Mn	%Cu	%Zn	%Ti	%Mg
EN AB-43500	9.0-11.5	<0.2	0.4-0.8	<0.03	<0.07	<0.15	0.15-0.6
1	9.89	0.16	0.5	<0.03	<0.03	0.03	0.29
2	9.9	0.16	0.5	0.07	<0.03	0.03	0.29
3	9.81	0.17	0.5	0.13	<0.03	0.03	0.29
4	9.9	0.17	0.5	0.13	0.11	0.03	0.29
5	9.78	0.19	0.51	0.14	0.2	0.03	0.3
6	10.28	0.14	0.58	0.03	<0.03	0.06	0.16
7	10.4	0.21	0.58	0.03	<0.03	0.06	0.16
8	10.39	0.25	0.58	0.03	<0.03	0.06	0.16
9	10.3	0.26	0.61	0.03	<0.03	0.06	0.16
10	10.37	0.26	0.63	0.03	<0.03	0.06	0.16
11	10.32	0.14	0.56	0.03	<0.03	0.06	0.17
12	10.26	0.18	0.62	0.07	<0.03	0.07	0.17
13	10.27	0.21	0.6	0.06	<0.03	0.06	0.16
14	10.31	0.25	0.59	0.11	<0.03	0.06	0.16
15	10.42	0.29	0.6	0.12	<0.03	0.06	0.16

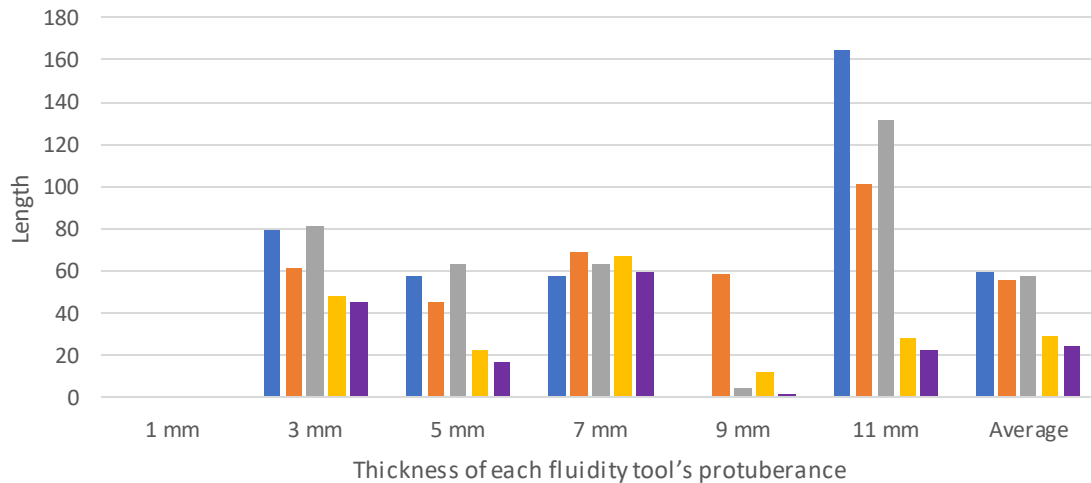


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Fluidity test result for 1st to 5th specimens



■ Sample 1 ■ Sample 2 ■ Sample 3 ■ Sample 4 ■ Sample 5

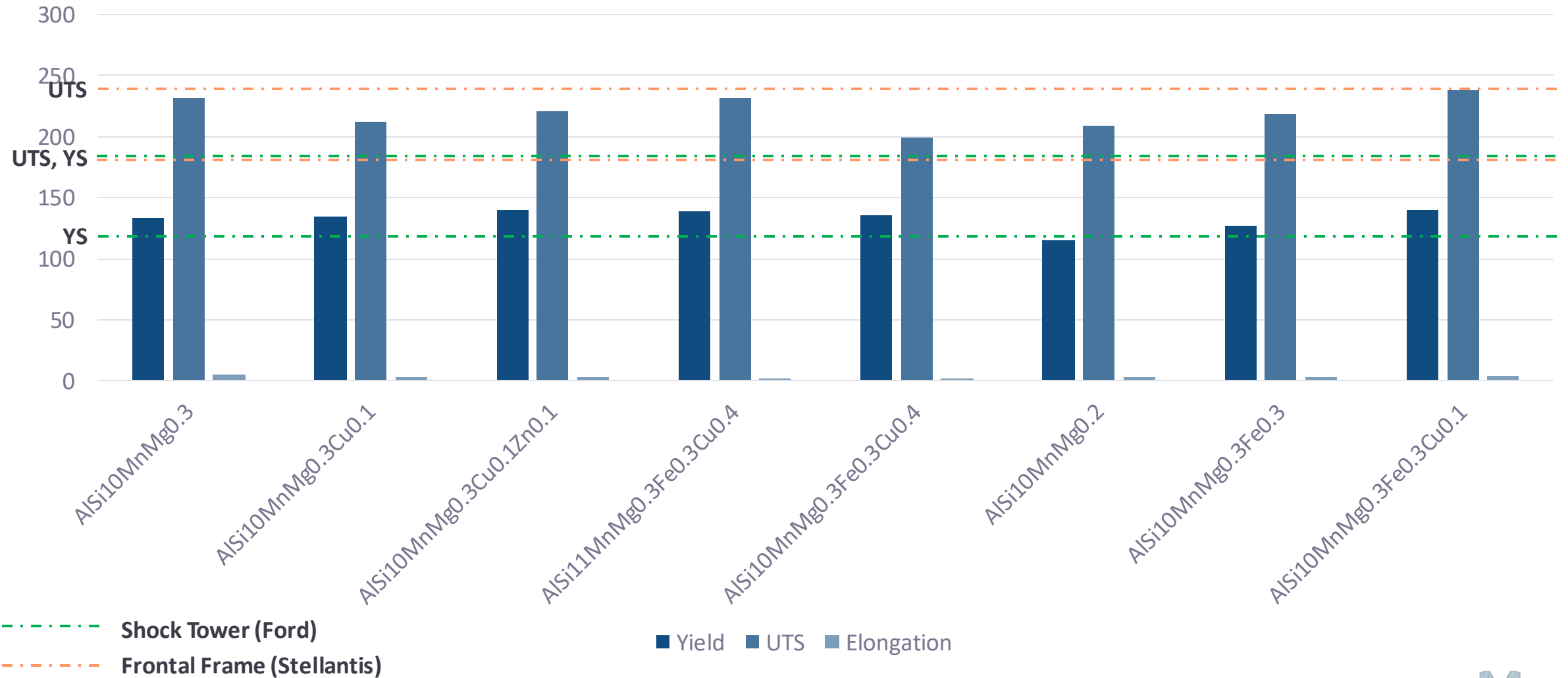
Alloy variant number	R _p [Mpa]	R _m [Mpa]	A ₂₅ [%]
1	92 ± 6	169 ± 4	5.9 ± 0.4
2	101 ± 7	177 ± 5	5.9 ± 1
3	98 ± 4	165 ± 16	3.8 ± 2.1
4	91 ± 2	173 ± 9	5.2 ± 1.3
5	105 ± 4	161 ± 27	3 ± 2.1



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HPDC ALLOY DEVELOPMENT








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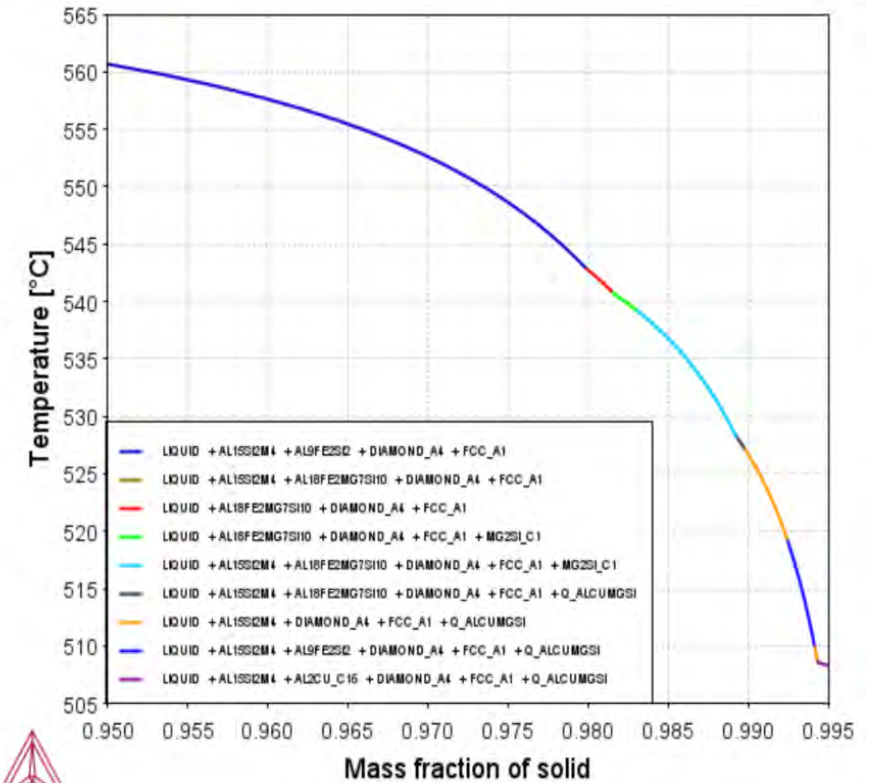


HPDC ALLOYS WITH REDUCED CRM CONTENT

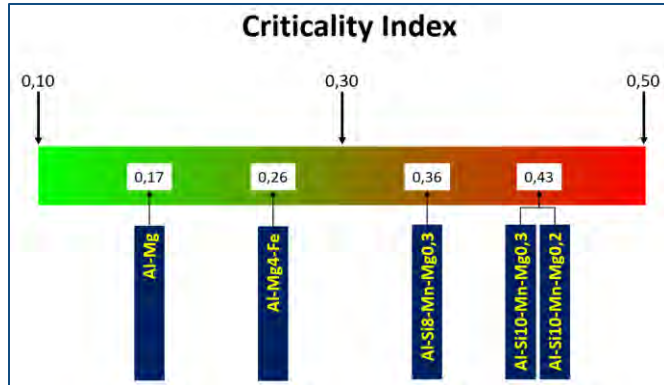
Hot Tearing

➔ TFR (Terminal Freezing Range):
95 to 100% of solidification

Conceptual area	Characteristic of phenomenon to be modelled	Category of model
CRM content	Criticality Index	Properly developed
Castability	Fluidity (as the inverse of viscosity)	 Thermo-Calc Software
	Solidification shrinkage	 + elaboration
	Slag/dross formation tendency	 + elaboration
	Die soldering tendency	 + elaboration
	Hot tearing tendency	 + elaboration



HPDC ALLOYS WITH REDUCED CRM CONTENT



Ranking for Processability

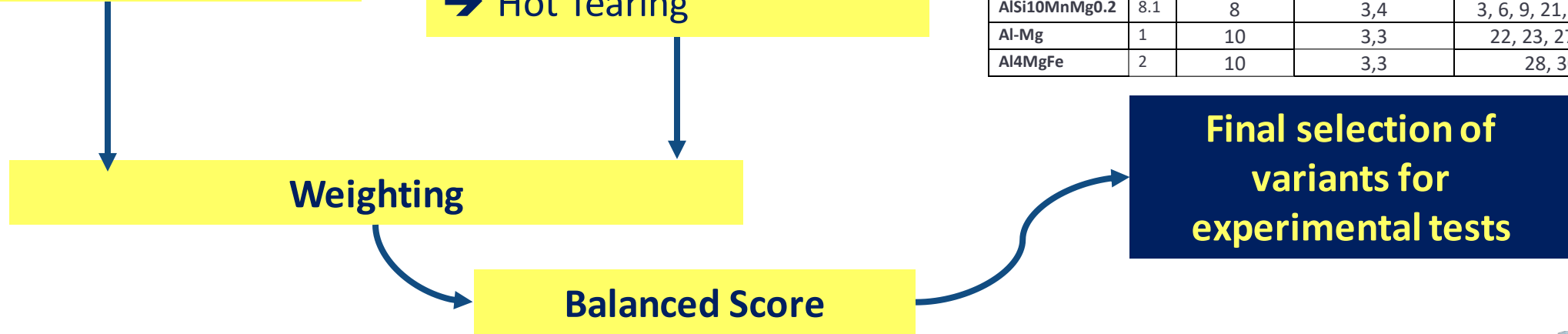
Attribution of weight to

- ➔ Viscosity/Fluidity
- ➔ Volume Shrinkage
- ➔ Sludge Factor
- ➔ Die soldering
- ➔ Hot Tearing

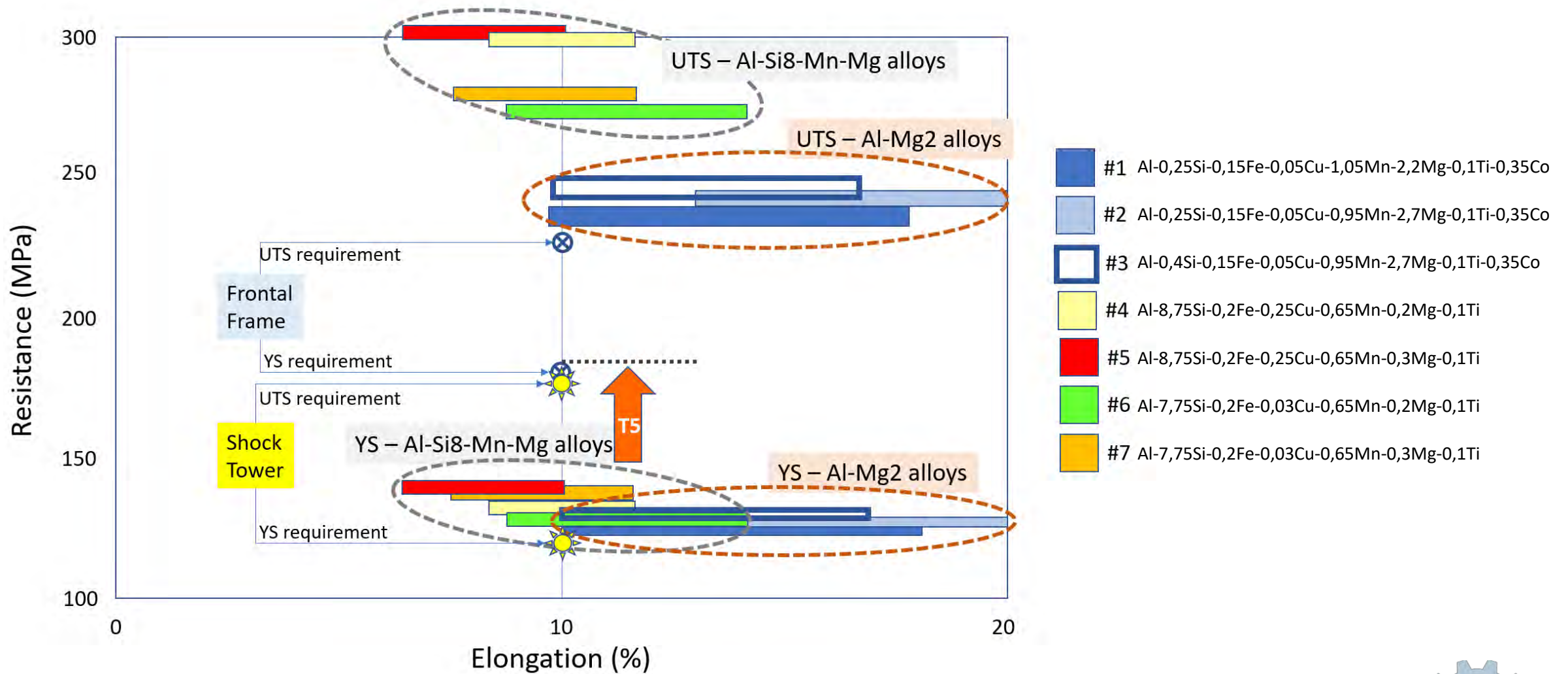
Ranking for Criticality

➔ Criticality Index

System	Set	RANKING	BALANCED SCORE	Suggested variants
AlSi8MnMg0.3	9	1	3,8	3, 6, 9, 21, 24, 27
AlSi10MnMg0.3	3	2	3,7	3, 6, 9, 21, 27
AlSi8MnMg0.3	10	2	3,7	3, 6, 9, 21, 24, 27
AlSi10MnMg0.2	6	4	3,6	3, 6, 9, 21, 24, 27
AlSi10MnMg0.2	7	4	3,6	3, 6, 9, 21, 24, 27
AlSi8MnMg0.3	11	4	3,6	3, 6, 9, 21, 24, 27
AlSi10MnMg0.3	4	6	3,5	3, 6, 9, 21, 27
AlSi10MnMg0.3	5	6	3,5	3, 6, 9, 21, 27
AlSi10MnMg0.2	8	8	3,4	3, 6, 9, 21, 24, 27
AlSi10MnMg0.2	8.1	8	3,4	3, 6, 9, 21, 24, 27
Al-Mg	1	10	3,3	22, 23, 27, 28,
Al4MgFe	2	10	3,3	28, 30



HPDC ALLOYS WITH REDUCED CRM CONTENT

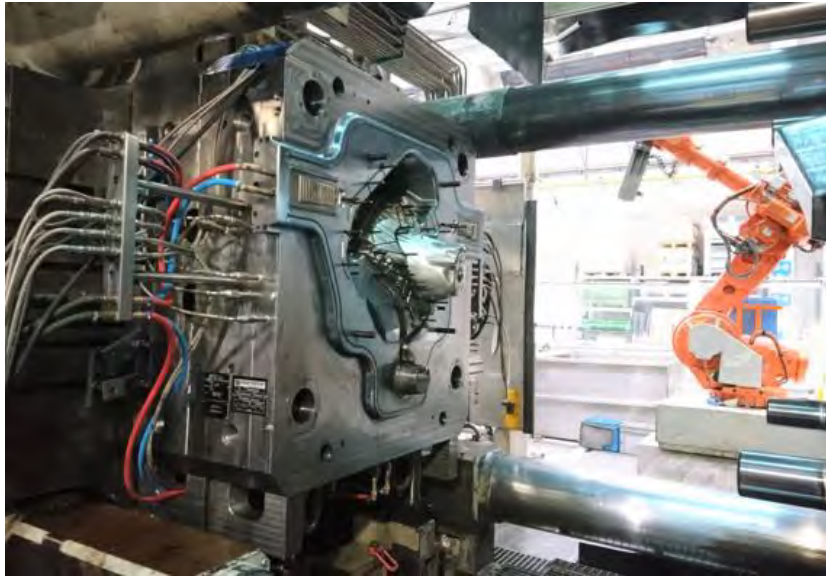


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INDUSTRIAL VALIDATION IN SHOCK-TOWER



F state (casted)

AlSi10MnMg

$R_{p0,2} = 133 \text{ MPa}$

$R_m = 268 \text{ MPa}$

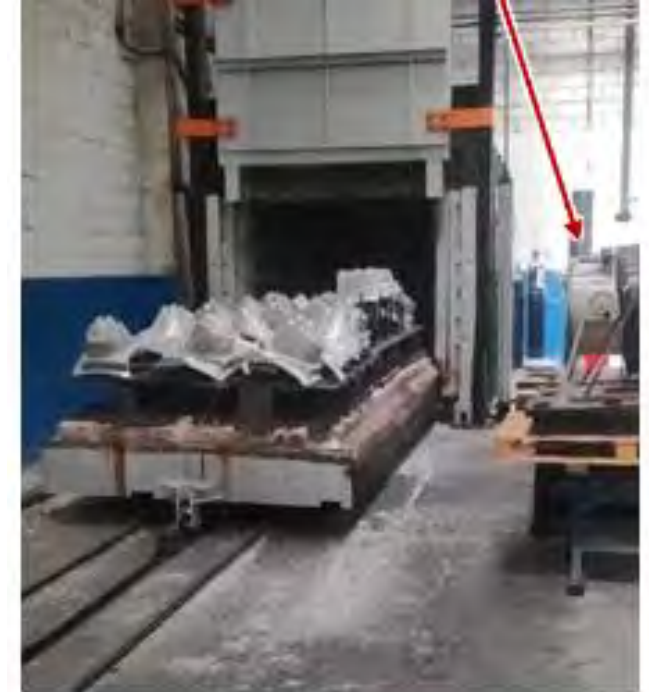
$A = 6,8 \%$

T7:
480°C/1h
+ air cooling
+ 230°C/2h

$R_{p0,2} = 129 \text{ MPa}$

$R_m = 200 \text{ MPa}$

$A = 12,7\%$



After HT



INDUSTRIAL VALIDATION IN SHOCK-TOWER



AlSi10MnMg

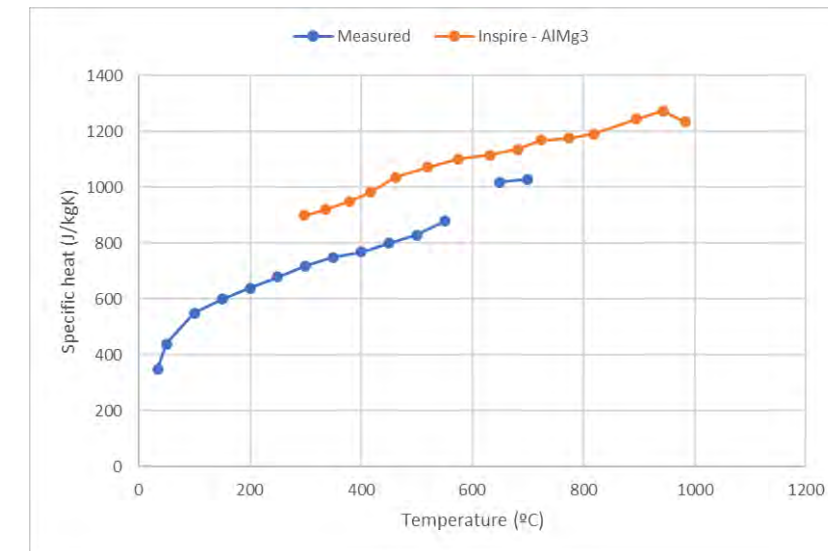
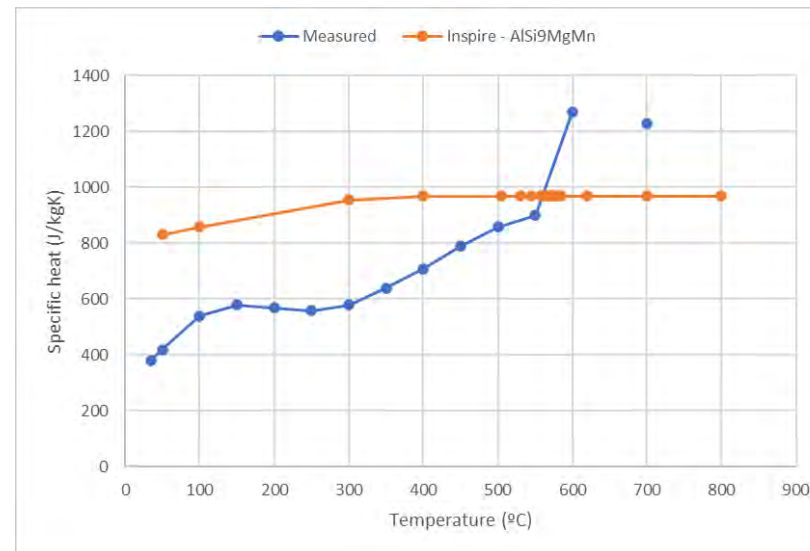
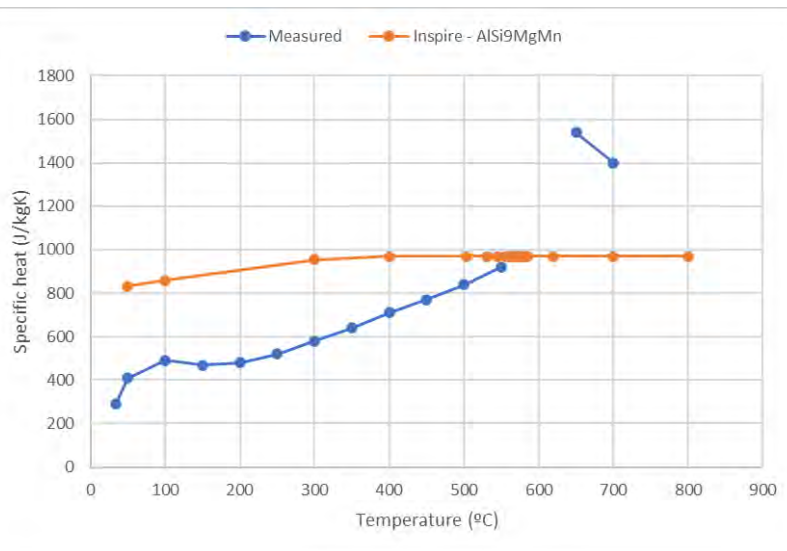
	Measured – Variant 6	Inspire – AlSi9MgMn
Latent heat (J/kg)	714825	417000
Liquidus temperature (°C)	599,8	590
Solidus temperature (°C)	589,8	550

AlSi8MnMg

	Measured – Variant 7	Inspire – AlSi9MgMn
Latent heat (J/kg)	677129	417000
Liquidus temperature (°C)	599,0	590
Solidus temperature (°C)	588,6	550

AlMg2

	Measured – Variant 12	Inspire – AlMg3
Latent heat (J/kg)	612828	400000
Liquidus temperature (°C)	664,3	640
Solidus temperature (°C)	636,7	590

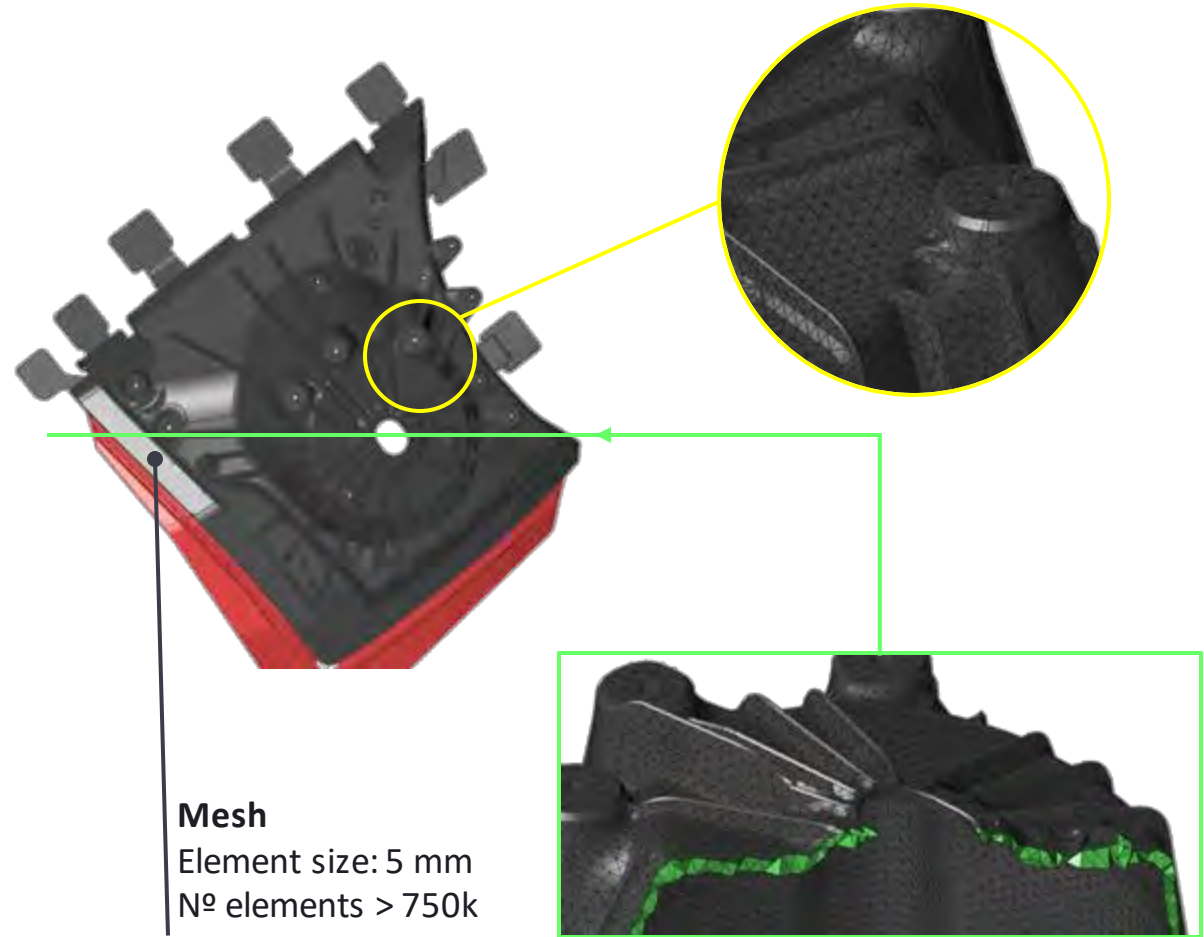
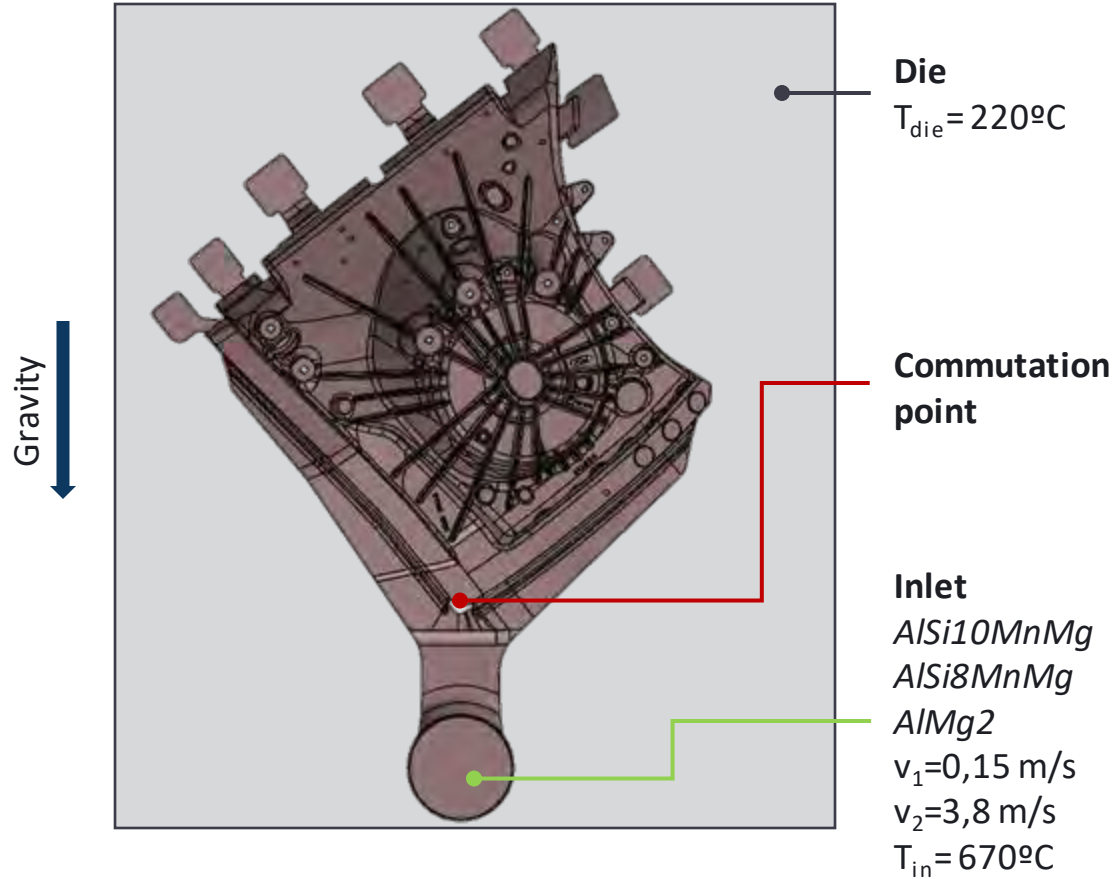


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INDUSTRIAL VALIDATION IN SHOCK-TOWER

Shock tower (EDERTEK): Geometry and mesh

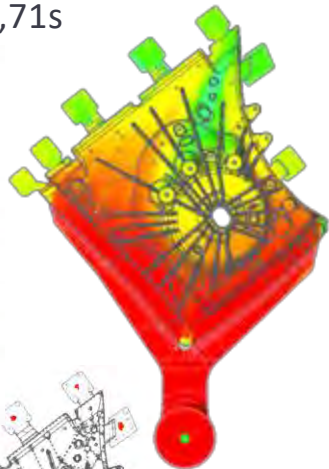
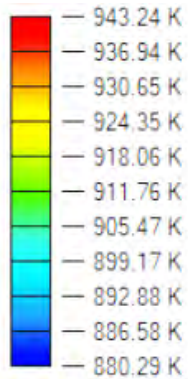


INDUSTRIAL VALIDATION IN SHOCK-TOWER

Shock tower (EDERTEK): Thermal conductivity, viscosity and density were obtained from InspireCast data base (AlSi9MgMn). All the other properties required by the software were determined experimentally from parts produced with the alloy variant.

AlSi10MnMg

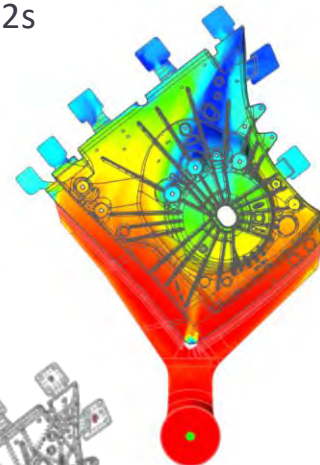
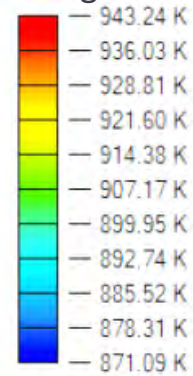
Filling time=0,71s



$\Delta T=63^{\circ}\text{C}$

AlSi8MnMg

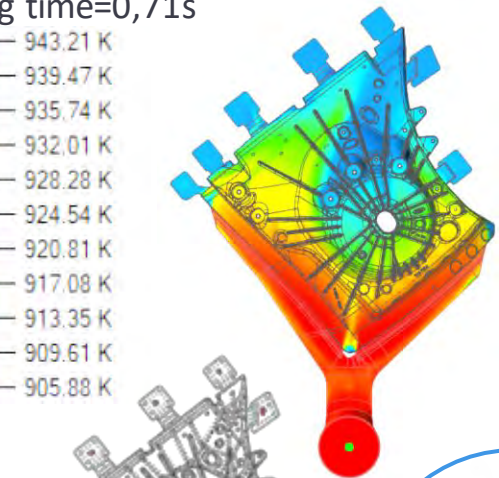
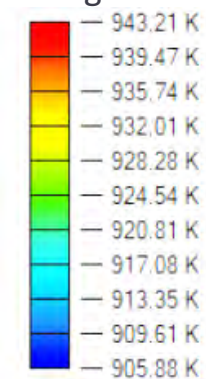
Filling time=0,72s



$\Delta T=72,2^{\circ}\text{C}$

AMg2

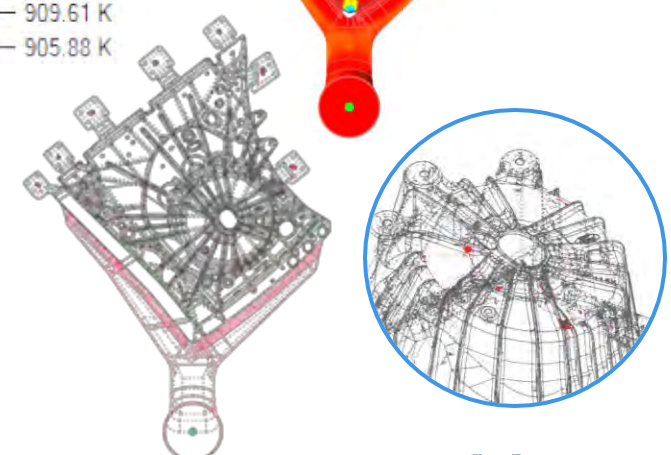
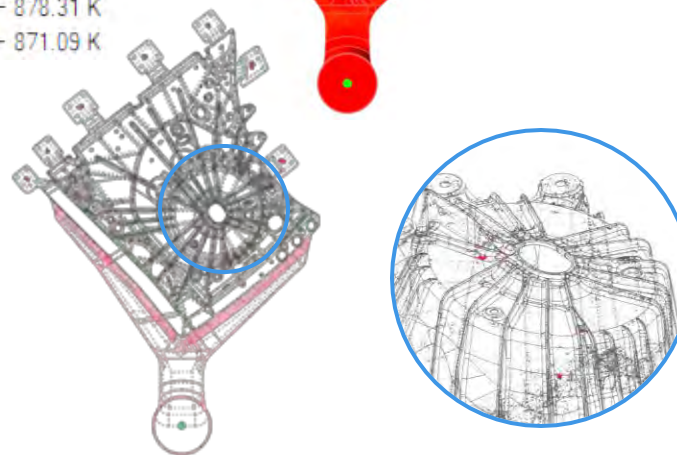
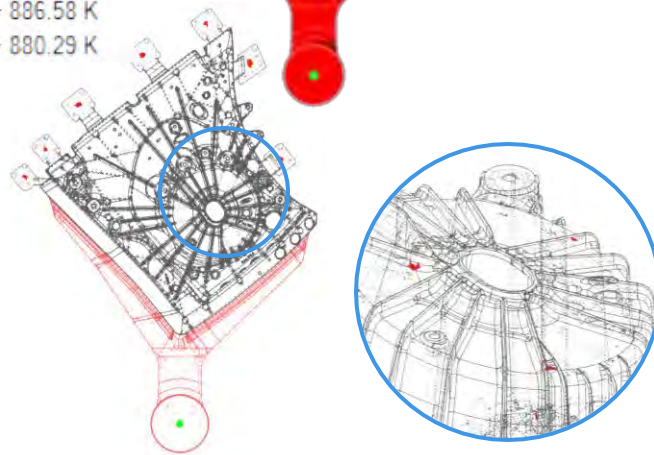
Filling time=0,71s



$\Delta T=37,3^{\circ}\text{C}$

FILLING

SOLIDIFICATION



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INDUSTRIAL VALIDATION IN SHOCK-TOWER

Mechanical properties (tensile test)

AlSi10MnMg Standard
(variant 1)

AlSi10MnMgFe0,3
(Variant6)

AlSi8MnMg
(Variant7)

AlMg2
(Variant 12)

F state (casted)

$R_{p0,2} = 133 \text{ MPa}$
 $R_m = 268 \text{ MPa}$
 $A = 6,8 \%$

$R_{p0,2} = 137 \text{ MPa}$
 $R_m = 264 \text{ MPa}$
 $A = 6\%$

$R_{p0,2} = 122 \text{ MPa}$
 $R_m = 248 \text{ MPa}$
 $A = 8,7 \%$

$R_p = 115 \text{ MPa}$
 $R_m = 205 \text{ MPa}$
 $A = 10\%$ (mean value, but with high dispersion)

T7:
480°C/1h
+air cooling
+ 230°C/2h

T7:
480°C/1h
+air cooling
+ 230°C/2h

T0_a:
320°C/1h

T0_b:
380°C/1h



After HT

$R_{p0,2} = 129 \text{ MPa}$
 $R_m = 200 \text{ MPa}$
 $A = 12,7\%$

$R_{p0,2} = 131 \text{ MPa}$
 $R_m = 185 \text{ MPa}$
 $A = 12,2\%$

$R_{p0,2} = 119 \text{ MPa}$
 $R_m = 216 \text{ MPa}$
 $A = 7,5\%$

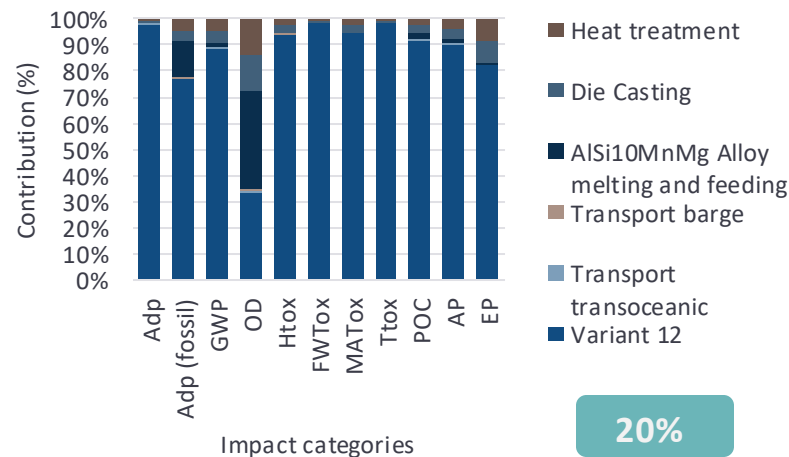
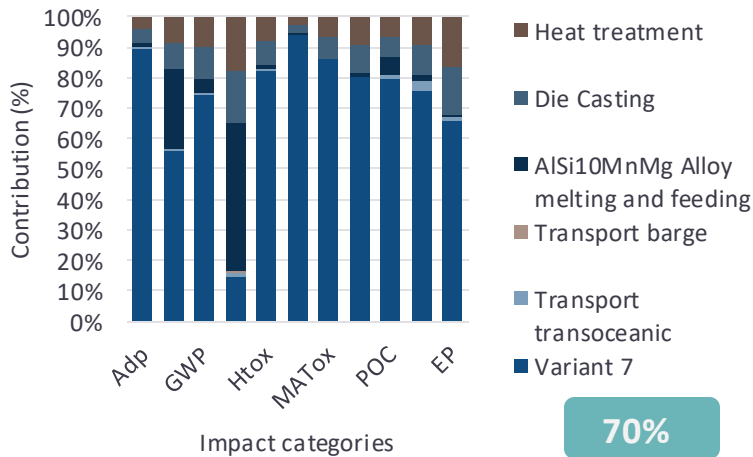
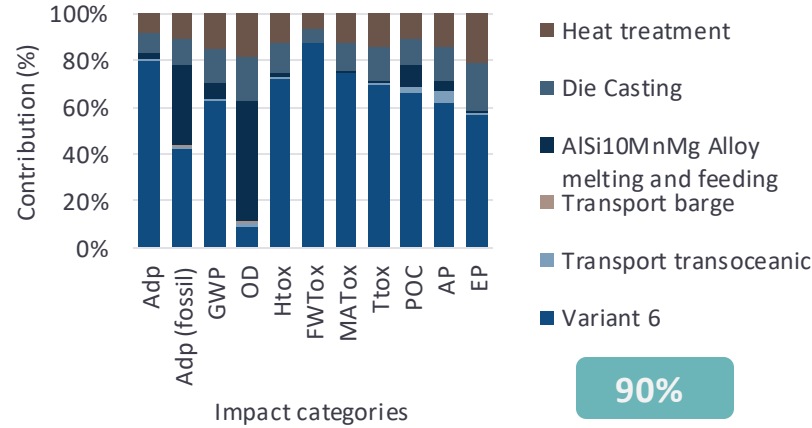
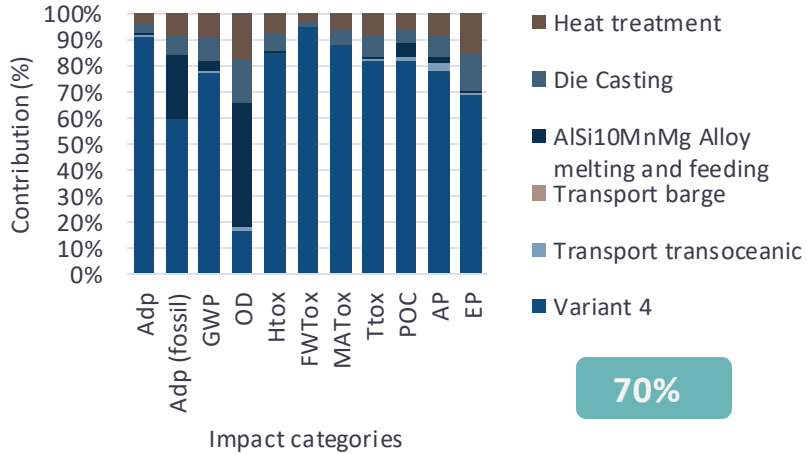
$R_{p0,2} = 100 \text{ MPa}$
 $R_m = 184 \text{ MPa}$
 $A = 11,4\%$

No improvement

Improvement in elongation, but $R_p < 120 \text{ MPa}$



INDUSTRIAL VALIDATION IN SHOCK-TOWER



HPDC	TOTAL Shock Tower Baseline	TOTAL Shock Tower Variant 4	TOTAL Shock Tower Variant 6	TOTAL Shock Tower Variant 7	TOTAL Shock Tower Variant 12
Abiotic depletion	2,69E-03	2,34E-05	1,03E-05	2,04E-05	1,05E-04
Abiotic depletion (fossil fuels)	8,18E+01	4,08E+01	2,89E+01	3,75E+01	7,21E+01
Global warming (GWP100a)	7,33E+00	3,15E+00	1,89E+00	2,80E+00	6,30E+00
Ozone layer depletion (ODP)	5,02E-07	1,87E-07	1,72E-07	1,82E-07	2,33E-07
Human toxicity	5,51E+00	2,18E+00	1,22E+00	1,92E+00	5,64E+00
Fresh water aquatic ecotox.	2,66E+01	7,88E+00	3,15E+00	6,84E+00	2,17E+01
Marine aquatic ecotoxicity	2,52E+04	8,64E+03	4,20E+03	7,47E+03	1,98E+04
Terrestrial ecotoxicity	1,53E-02	1,01E-02	5,91E-03	8,99E-03	1,27E-01
Photochemical oxidation	2,37E-03	9,23E-04	4,88E-04	8,02E-04	2,00E-03
Acidification	3,93E-02	1,60E-02	9,22E-03	1,42E-02	3,36E-02
Eutrophication	1,38E-02	6,48E-03	4,68E-03	5,98E-03	1,13E-02

GWP 57,1% 74,2% 61,8% 14,0%

Co
Mg
Cu



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SHEET METAL ALLOY DEVELOPMENT

	%Si	%Fe	%Cu	%Mn	%Mg	%Cr	Ti	%Zn
6181A (T4)	0.85	0.29	0.13	0.30	0.76	<0.03	<0.03	0.06

Alloy	Variant	Si	Fe	Cu	Mn	Mg	Cr	Zn	Ti
6181A	Tipo0 (50 % recycled)	0,89	0,21	0,09	0,01	0,69	0,01	0,02	0,02
6181A	Tipo1 (70% recycled)	1	0,3	0,19	0,28	0,8	0,02	0,07	0,03
6181A	Tipo2 (85% recycled)	1,1	0,35	0,19	0,3	0,84	0,02	0,08	0,03

	%Si	%Fe	%Cu	%Mn	%Mg	%Cr	Ti	%Zn
5754 (EN-573-3)	0.25	0.40	0.1	0.5	2.6-3.6	0.3	0.2	0.15

Alloy	Variant	Si	Fe	Cu	Mn	Mg	Cr	Zn	Ti
5754	Tipo1 (65% recycled)	0,29	0,31	0,08	0,21	2,88	0,03	0,02	0,03
5754	Tipo2 (80% recycled)	0,32	0,38	0,07	0,24	2,91	0,04	0,03	0,03



SHEET METAL ALLOY DEVELOPMENT



Tensile Properties

COLD FORMING ALLOYS

	Rp [MPa]	Rm [MPa]	A%
5754 - Type1	97	210	22.5
5754 - Type2	100	212	22.3
6181A - type0	136	252	21
6181A - type1	163	276	24
6181A -type2	172	282	24

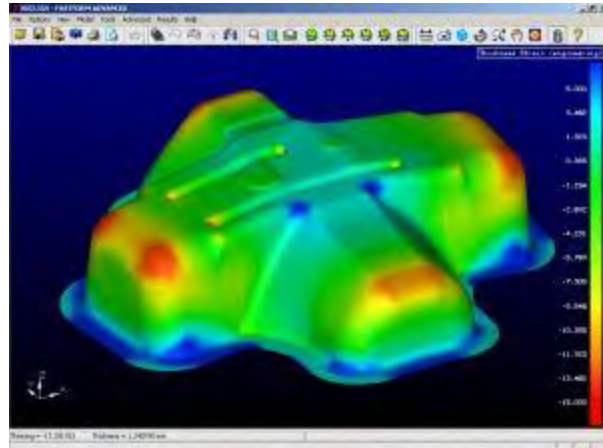
HOT FORMING ALLOYS

	Rp [MPa]	Rm [MPa]	A%
6181A - type0	287	345	18.0
6181A - type1	287	346	16.4
6181A -type2	290	345	18.0
6111	301	376	17



SHEET METAL ALLOY DEVELOPMENT

Formability Parameters



Dir.	Rp0.2 [MPa]	Rm [MPa]	Ag [%]	A50 [%]	n	r	\bar{r}	Δr
5754 Type 1								
0°	101 ± 2	215 ± 1	16.0 ± 0.7	19.5 ± -	0.29 ± 0.01	0.58 ± 0.03	0.75	-0.21
45°	95 ± 1	206 ± 1	20.0 ± 0.3	23.3 ± 0.8	0.28 ± 0.01	0.86 ± 0.02		
90°	97 ± 1	209 ± 0	20.2 ± 1.6	25.0 ± 1.2	0.27 ± 0.00	0.71 ± 0.01		
5754 type 2								
0°	105 ± 0	219 ± 2	17.2 ± 1.0	19.4 ± 1.1	0.28 ± 0.00	0.61 ± 0.01	0.77	-0.23
45°	97 ± 1	209 ± 2	20.9 ± 1.2	24.8 ± 0.9	0.27 ± 0.00	0.89 ± 0.01		
90°	99 ± 1	210 ± 0	19.1 ± 0.4	22.7 ± -	0.27 ± 0.00	0.71 ± 0.01		

Dir.	Rp0.2 [MPa]	Rm [MPa]	Ag [%]	A50 [%]	n	r	\bar{r}	Δr
6181A Type 0								
0°	127 ± 1	211 ± 3	15.9 ± 1.0	18.1 ± 1.3	0.22 ± 0.01	0.60 ± 0.04	0.76	0.06
45°	100 ± 3	170 ± 2	15.3 ± 0.9	-	0.23 ± 0.01	0.73 ± 0.07		
90°	129 ± 1	230 ± 3	17.3 ± 0.3	-	0.25 ± 0.01	0.98 ± 0.07		
6181A Type 1								
0°	125 ± 4	203 ± 2	17.0 ± 0.6	19.4 ± 0.1	0.21 ± 0.01	0.70 ± 0.06	0.56	0.10
45°	127 ± 4	215 ± 7	15.4 ± 4.6	19.6 ± 5.5	0.24 ± 0.01	0.52 ± 0.03		
90°	127 ± 3	219 ± 3	18.3 ± 0.8	-	0.25 ± 0.01	0.52 ± 0.01		
6181A Type 2								
0°	137 ± 1	239 ± 2	17.1 ± 0.6	-	0.25 ± 0.01	0.69 ± 0.03	0.53	0.23
45°	131 ± 2	234 ± 2	21.3 ± 1.3	24.5 ± 2.0	0.25 ± 0.01	0.42 ± 0.04		
90°	122 ± 4	207 ± 3	15.7 ± 3.0	21.7 ± -	0.25 ± 0.01	0.61 ± 0.07		



SHEET METAL ALLOY DEVELOPMENT

Essential Work of Fracture

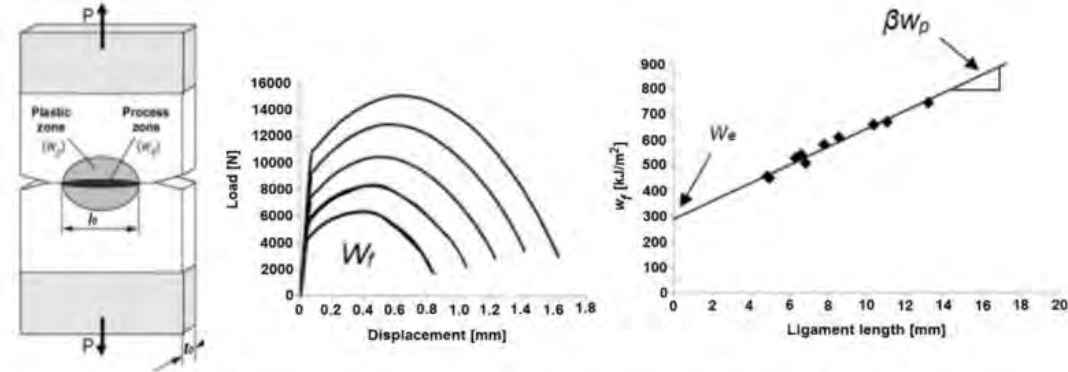


Figure 3.8: Test geometry and methodology for determination of the Essential Work of Fracture.

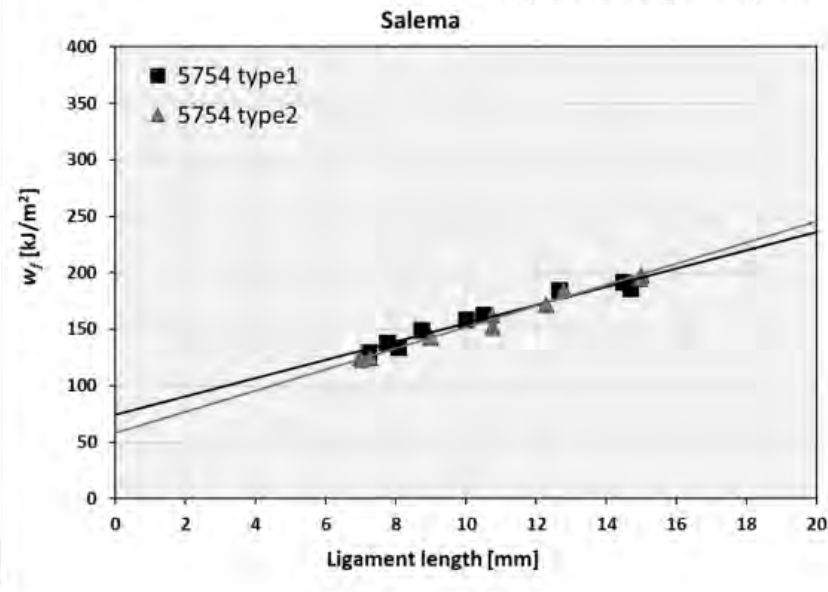


Figure 3.10: EWF results for 5754 variants

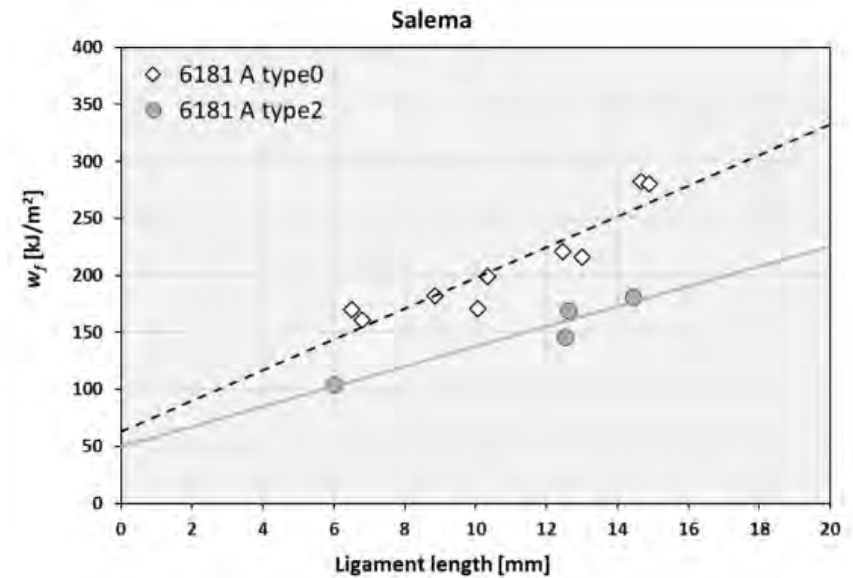


Figure 3.13: EWF results for 6181A; comparison of Type 0 and 2.

SHEET METAL ALLOY DEVELOPMENT



Cold Formability

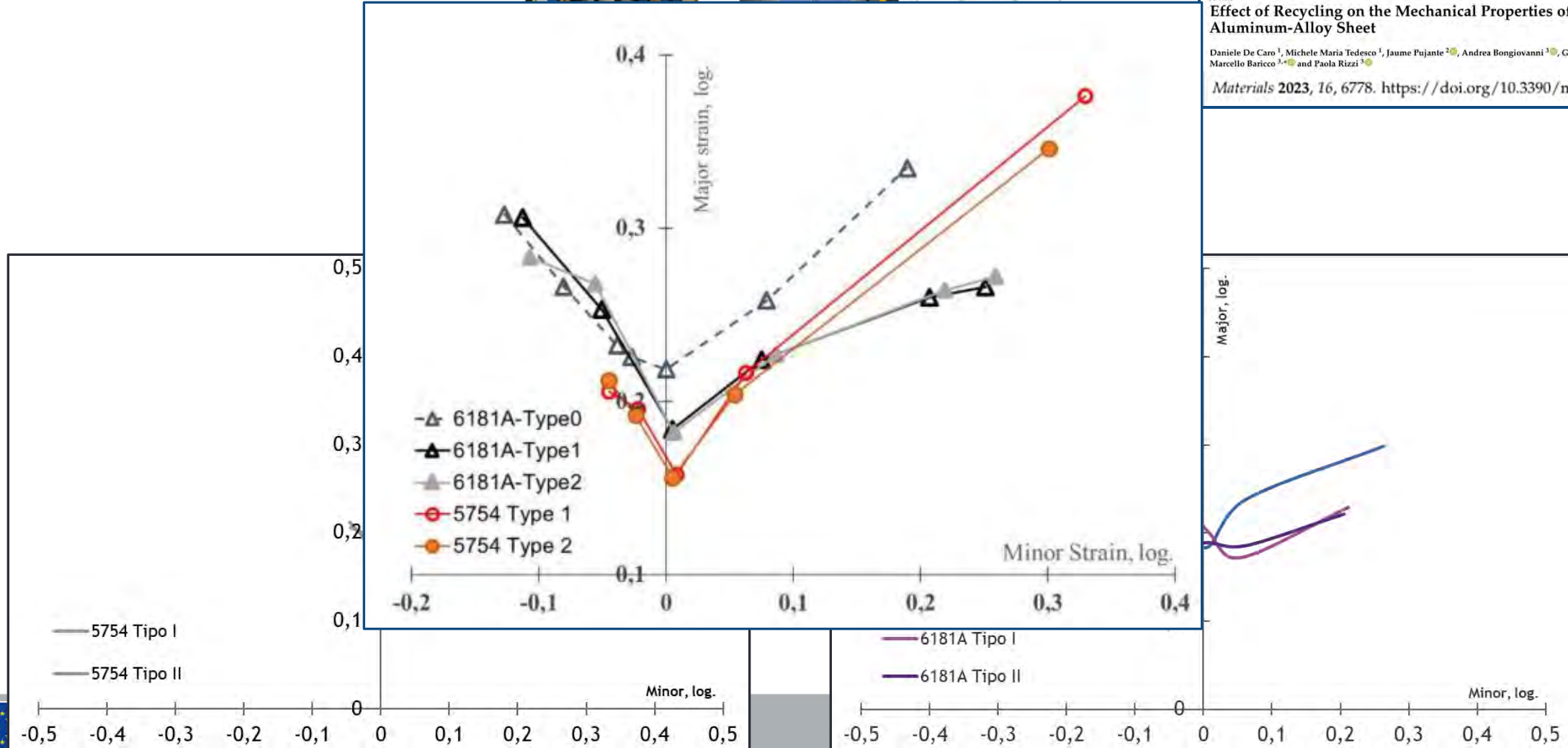


materials MDPI

Article
Effect of Recycling on the Mechanical Properties of 6000 Series Aluminum-Alloy Sheet

Daniele De Caro ¹, Michele Maria Tedesco ¹, Jaume Pujante ², Andrea Bongiovanni ³, Giovanni Sbraga ⁴,
 Marcello Baricco ³ and Paola Rizzi ³

Materials **2023**, *16*, 6778. <https://doi.org/10.3390/ma16206778>



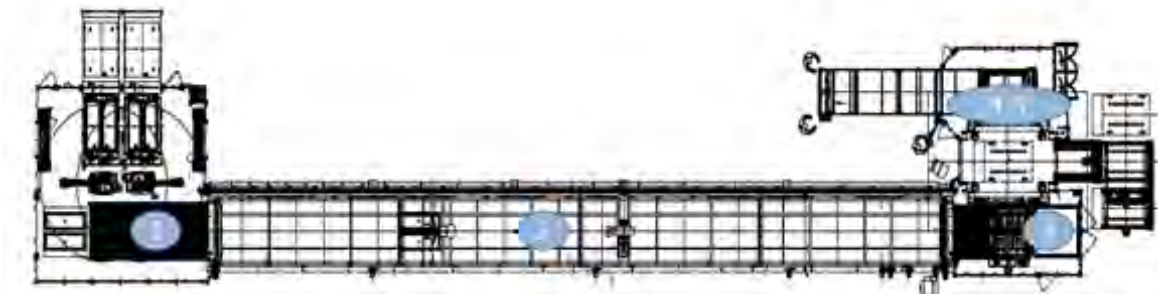
INDUSTRIAL VALIDATION IN HOT STAMPING

- PROJECT TARGET

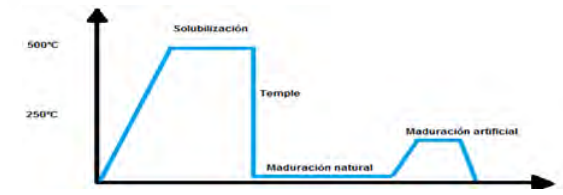
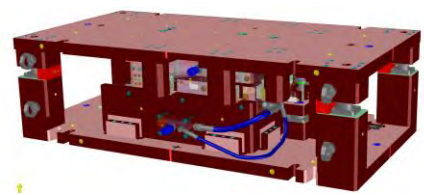
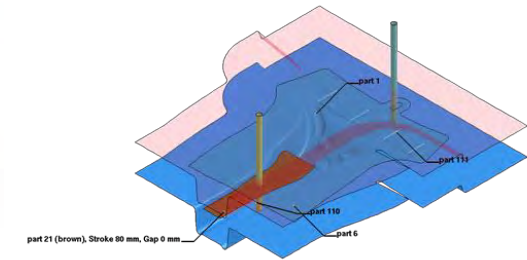
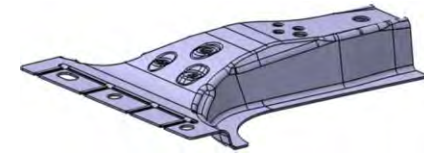
- Use of aluminum with high recycle content
 - 6111 85%
 - 6181A 85%

Alloy	Rp [MPa]	Rm [MPa]	A [%]
6181A T4	110-140	205-240	12 a 23
6181A T6	220-310	260-375	4 a 13
6111 T4	150-180	270-290	20-26
6111 T6	250-310	360-390	8-14

- Process implementation in the current Assets.



INDUSTRIAL VALIDATION IN HOT STAMPING



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.



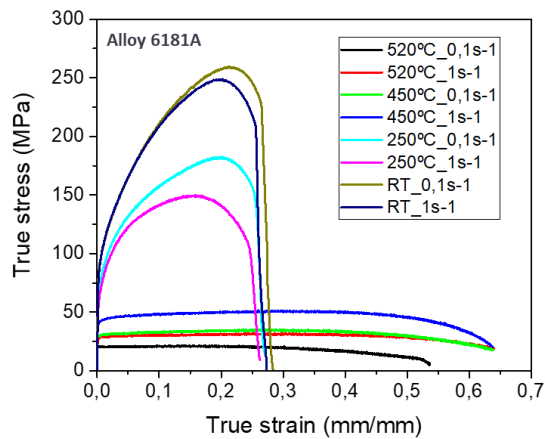
INDUSTRIAL VALIDATION IN HOT STAMPING

- PROCESS SIMULATION

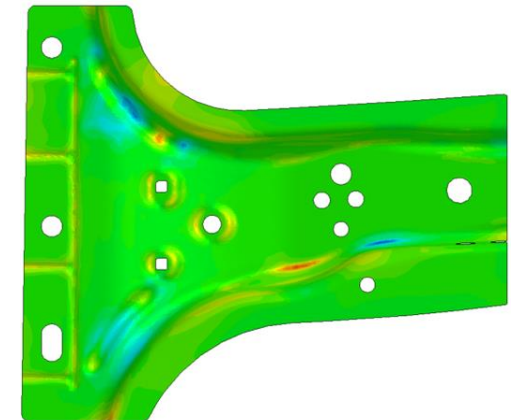
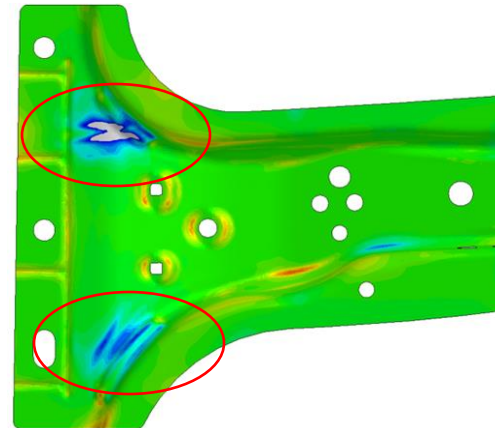
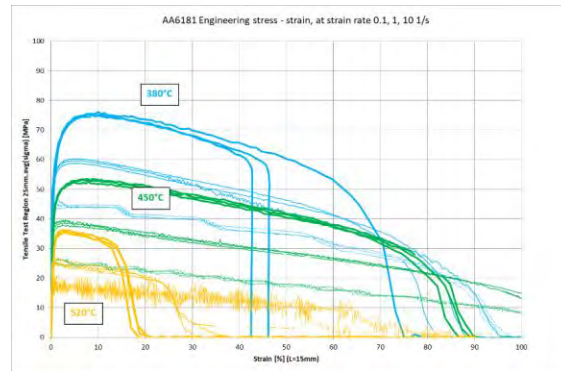
EURECAT – GESTAMP LABORATORY TEST

GESTAMP PART PROCESS SIMULATION

TENSILE TEST



FRICTION TEST



MATERIAL DATA CARD



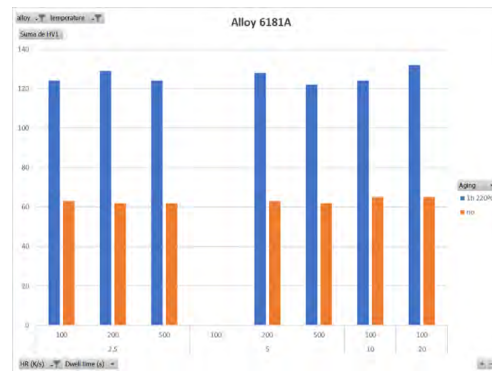
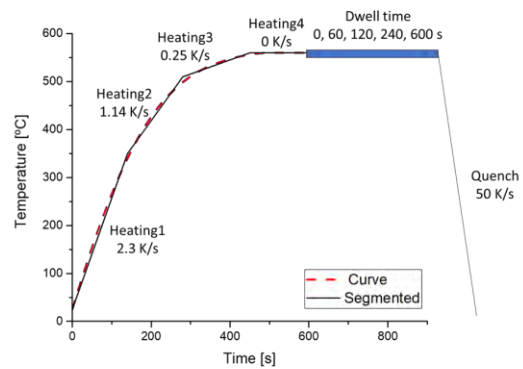
INDUSTRIAL VALIDATION IN HOT STAMPING



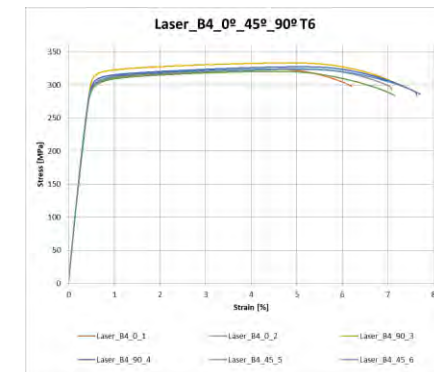
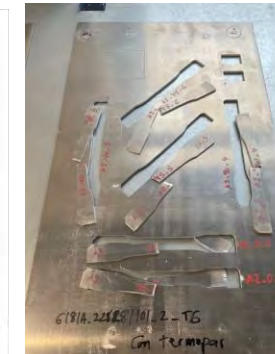
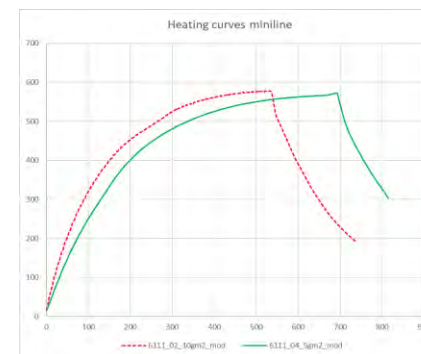
- PROCESS PARAMETER



EURECAT LABORATORY TEST



GESTAMP LINE



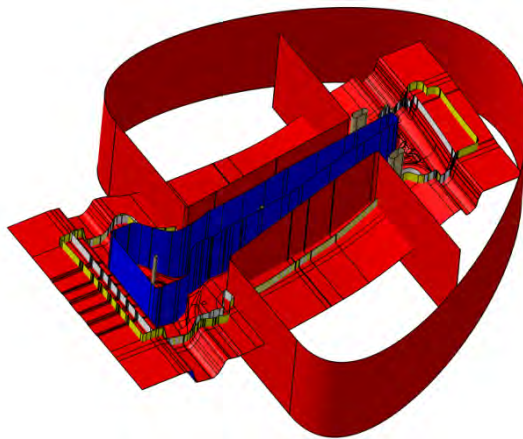
The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.



INDUSTRIAL VALIDATION IN HOT STAMPING

- TOOLING DESIGN & PRODUCTION

GESTAMP TOOLING "SURFACE"

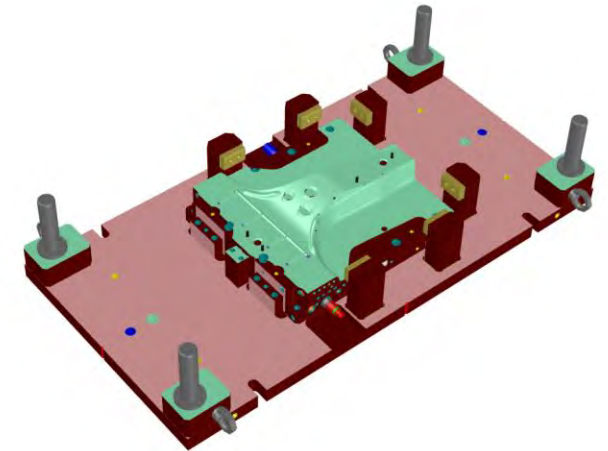
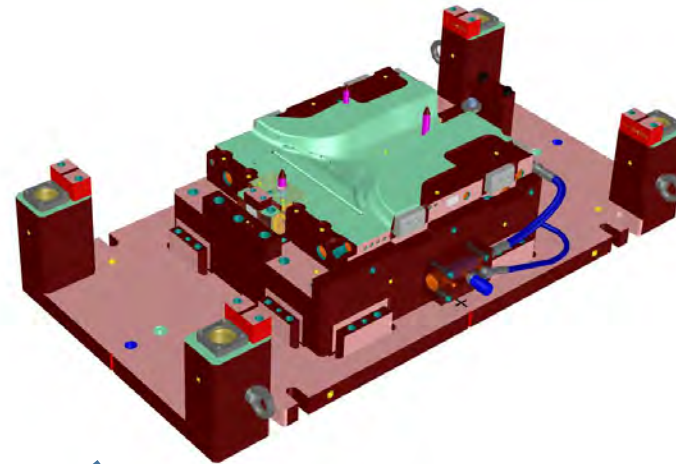


Tool_XXXX_YYYY.stp contains the following data:

- Upper die = Red
- Lower die = Blue
- Blank guide (optional) = Brown
- Upper split surfaces (optional) = Red
- Lower split surfaces (optional) = Blue
- Upper limit for fine/coarse milling = White
- Upper binder limit for fine/coarse milling = Pink
- Lower limit for fine/coarse milling = Yellow
- Lower binder limit for fine/coarse milling = Grey
- Splits for Tool SZ (obtained from Tooling) = Green

VIRTUAL

GESTAMP TOOLING MANUFACTURE

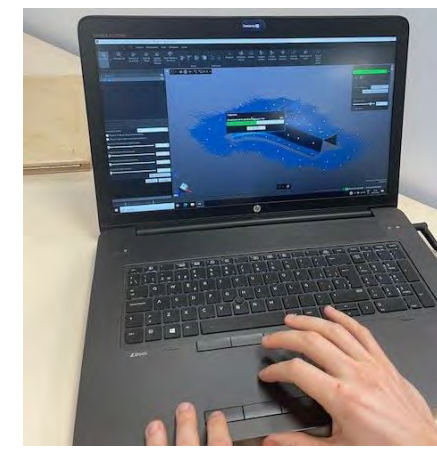
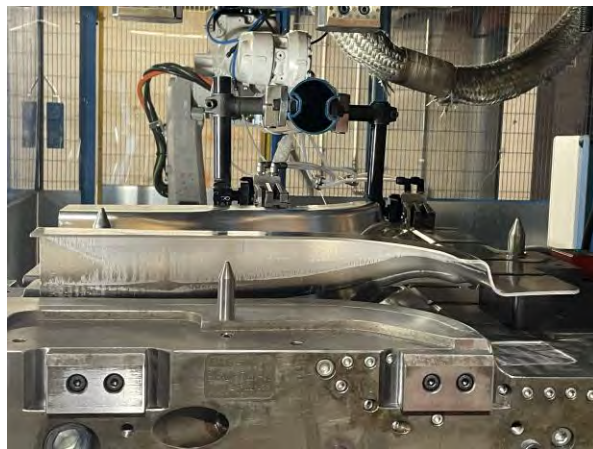


PHYSICAL



INDUSTRIAL VALIDATION IN HOT STAMPING

- PART PRODUCTION



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Manel da Silva, PhD

Technical Coordinator

manel.dasilva@eurecat.org



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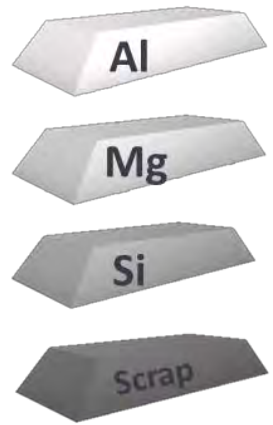
[*@salemaEU*](https://twitter.com/salemaEU)

Summary

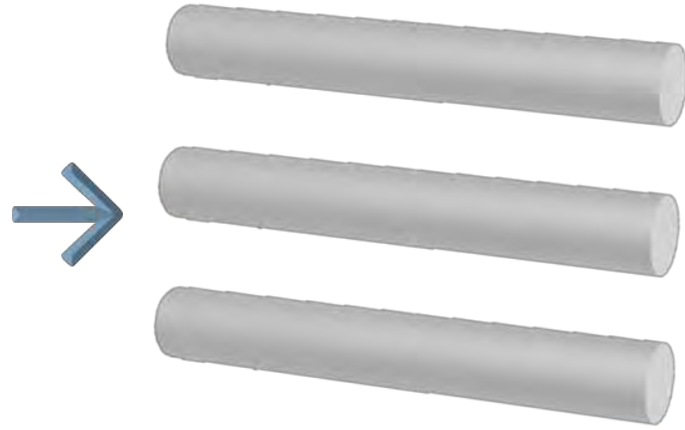
- Project introduction and video
- Scrap sorting system
- Development of HPDC SALEMA alloys
- Validation of HPDC SALEMA alloys in Shock Tower
- Alloy development and industrial validation in Hot Stamping
- Alloy development and industrial validation in extrusion
- Validation procedure of new alloys by an OEM



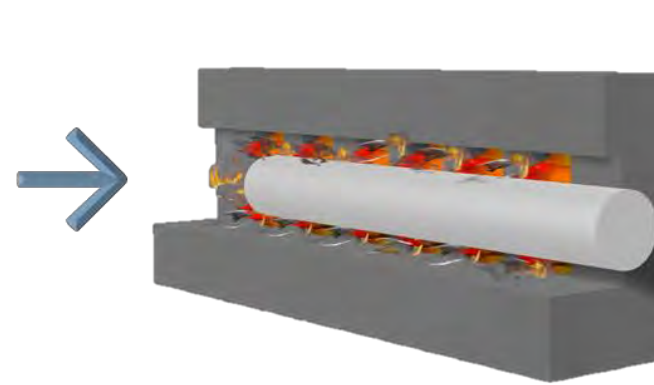
ALUMINIUM ALLOY EXTRUSION METHODOLOGY



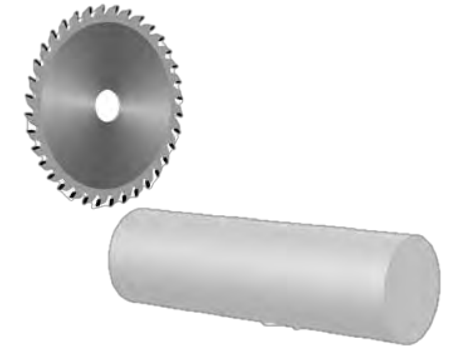
Alloying



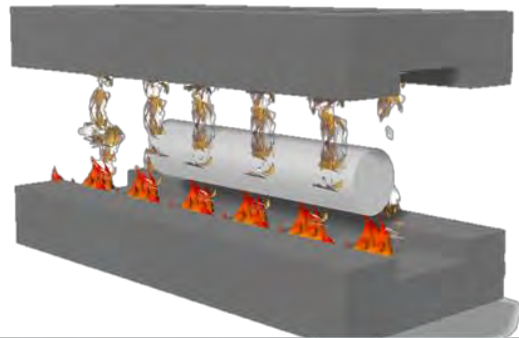
DC Casting



Homogenization



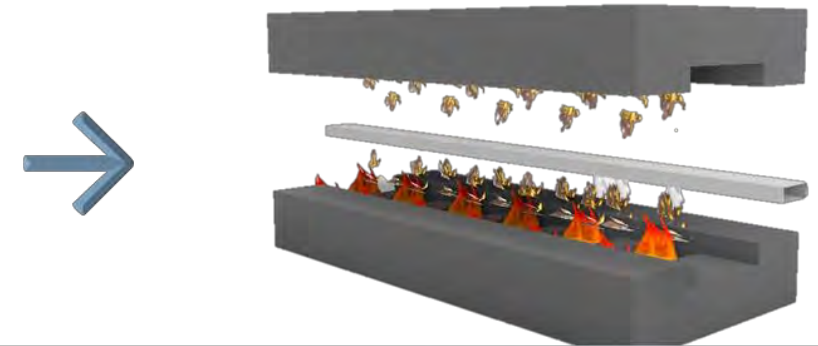
Cutting



Pre-heating



Direct Extrusion



Heat Treatment



EXTRUSION ALLOY DEVELOPMENT

	Variant	Content. wt. %										
		Si	Fe	Cu	Mn	Mg	Cr	Ni	Zn	Pb	Sn	Ti
6111	1	0.8-1.0	0-0.4	0.6-0.8	0.15-0.45	0.7-0.9	0-0.1	0.05	0-0.15	0.05	0.05	0-0.1
	2	0.6-0.8	0-0.4	0.7-0.9	0.15 - 0.45	0.5-0.7	0-0.1	0.05	0-0.15	0.05	0.05	0-0.1
	3	0.6-0.8	0-0.4	0.5-0.7	0.15-0.45	0.5-0.7	0-0.1	0.05	0-0.15	0.05	0.05	0-0.1
6063	1	0.4-0.6	0-0.35	0-0.1	0-0.15	0.5-0.7	0-0.1	0-0.05	0-0.1	0-0.05	0-0.05	0-0.1
	2	0.4-0.6	0-0.35	0.1-0.15	0.15-0.2	0.5-0.7	0-0.1	0-0.05	0.1-0.15	0-0.05	0-0.05	0.1-0.15
	3	0.4-0.6	0.35-0.45	0.15-0.2	0.2-0.25	0.5-0.7	0-0.1	0-0.05	0.1-0.15	0-0.03	0-0.03	0.1-0.15
6082	1	0.9-1.1	0-0.5	0-0.1	0.6-0.8	0.8-1	0-0.25	0-0.05	0-0.2	0-0.05	0-0.05	0-0.1
	2	0.9-1.1	0-0.5	0.1-0.15	0.6-0.8	0.8-1	0-0.25	0-0.05	0-0.2	0-0.05	0-0.05	0-0.1
	3	0.9-1.1	0-0.5	0.15-0.2	0.6-0.8	0.8-1	0-0.25	0-0.05	0-0.2	0-0.05	0-0.05	0.1-0.15



EXTRUSION ALLOY DEVELOPMENT

Different Scraps



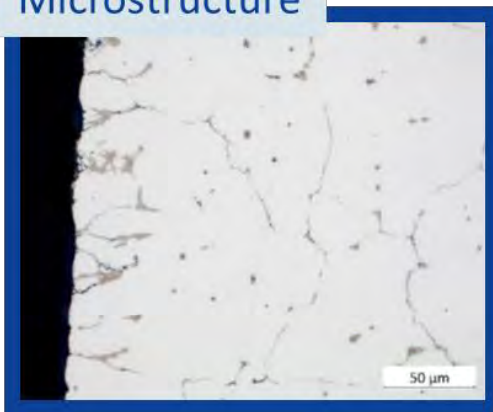
Lab-Scale Casting



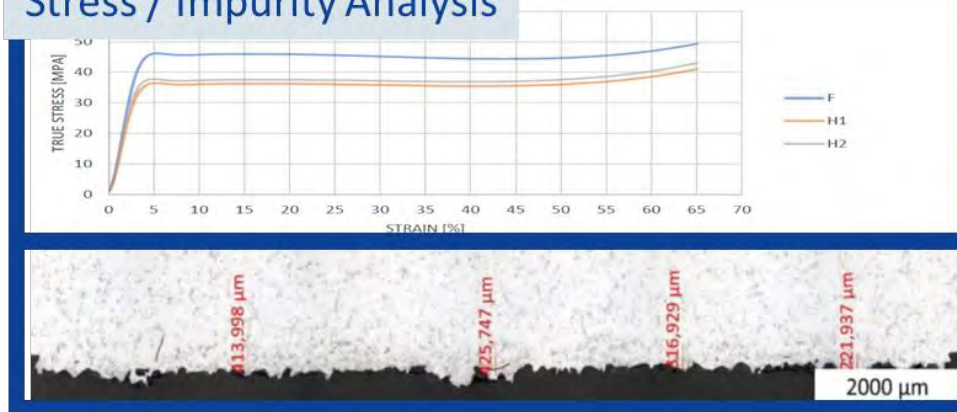
Final Billets



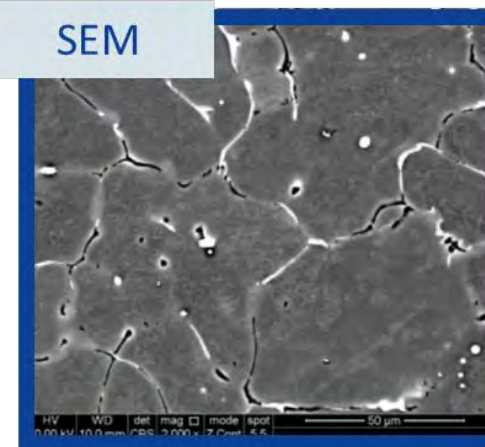
Microstructure



Stress / Impurity Analysis

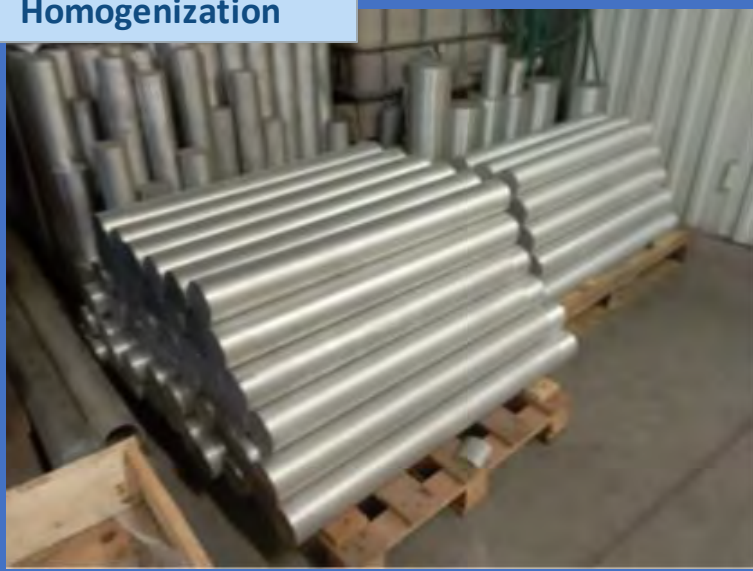


SEM



EXTRUSION ALLOY DEVELOPMENT

Homogenization



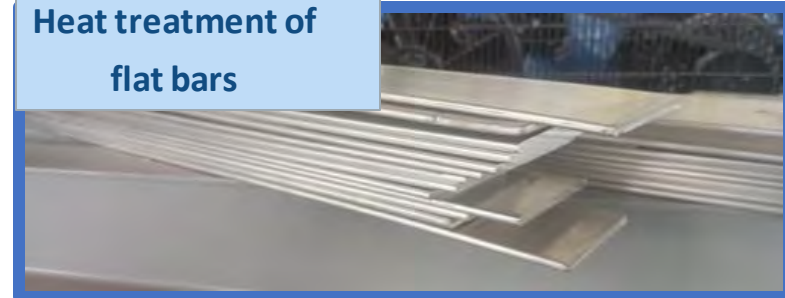
Optimization of extrusion



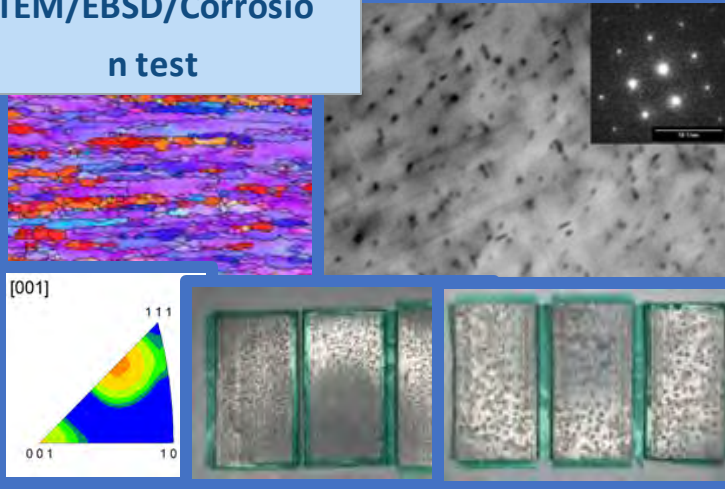
Extrusion die



Heat treatment of flat bars



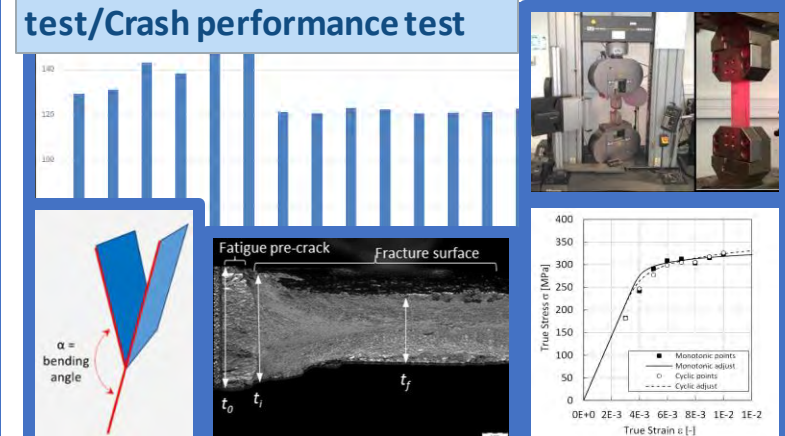
TEM/EBSD/Corrosion test



Tensile test/Bake paint test



Bending test/Fatigue test/Crash performance test



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.

EXTRUSION ALLOY DEVELOPMENT

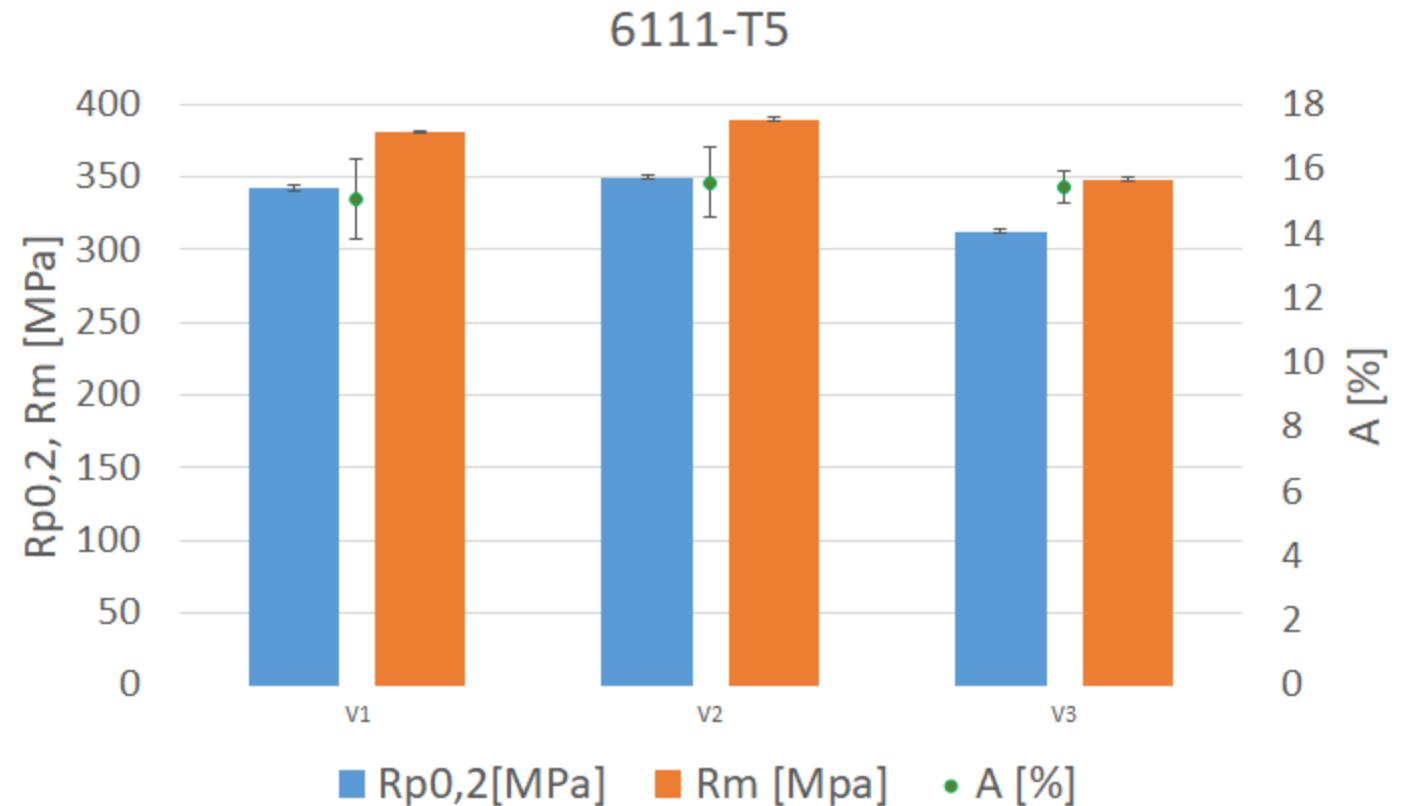
Low CRM 6111

6111	Si	Fe	Cu	Mn	Mg	Cr	Zn	Ti
Variant 1	0.935	0.070	0.779	0.284	0.861	0.0007	0.0045	0.0198
Variant 2	0.719	0.072	0.814	0.290	0.623	0.0010	0.0059	0.0198
Variant 3	0.708	0.073	0.547	0.285	0.629	0.0008	0.0043	0.0198

Static tensile test: EN ISO 6892-1:2020-05

- Crosshead speed1 = 0,75mm/min
- croshead speed2 = 5mm/min.
- Gauge length 50mm

	Rp0,2 [MPa]	Rm [Mpa]	A [%]
V1	342,7	381,3	15,1
V2	349,7	390,0	15,6
V3	312,7	348,7	15,5



EXTRUSION ALLOY DEVELOPMENT



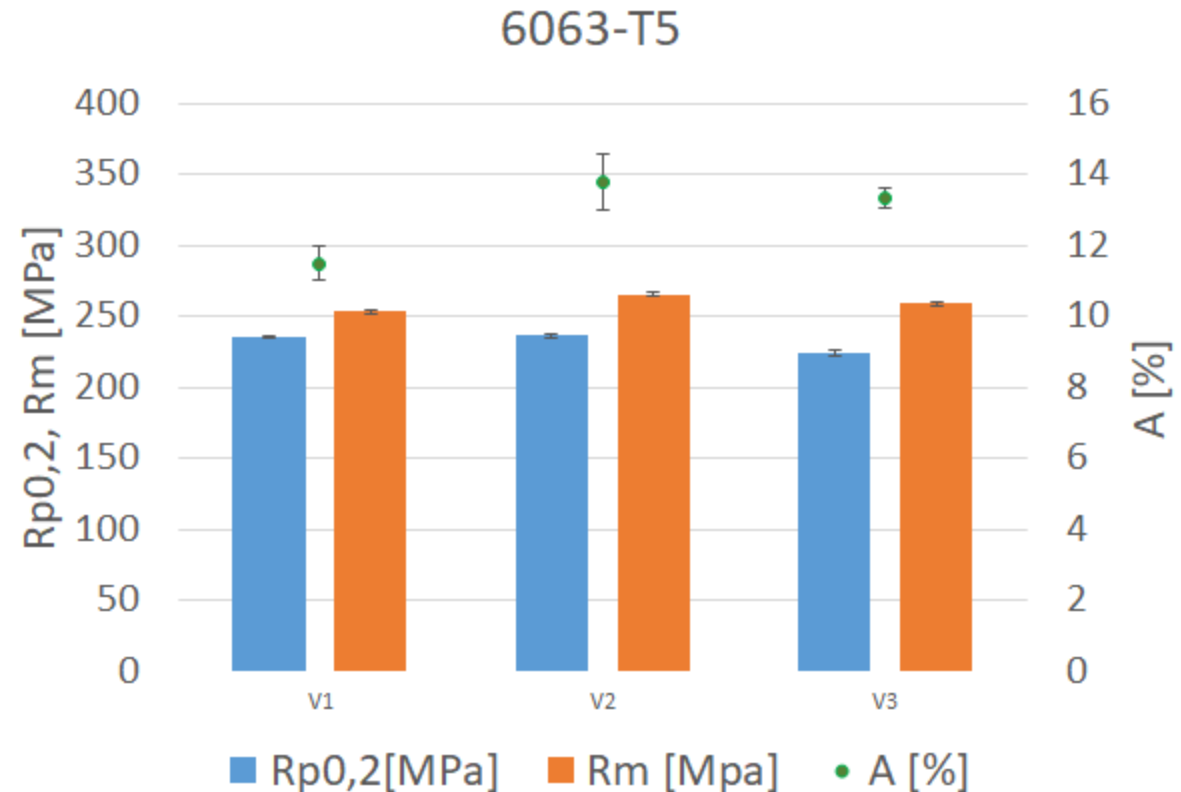
High scrap content 6063

6063	Si	Fe	Cu	Mn	Mg	Cr	Zn	Ti
Variant 1	0.539	0.217	0.026	0.090	0.514	0.022	0.060	0.0400
Variant 2	0.507	0.227	0.120	0.167	0.512	0.025	0.117	0.1490
Variant 3	0.509	0.398	0.173	0.200	0.524	0.025	0.122	0.1440

Static tensile test: EN ISO 6892-1:2020-05

- Crosshead speed1 = 0,75mm/min
- croshead speed2 = 5mm/min.
- Gauge length 50mm

	Rp0,2 [MPa]	Rm [Mpa]	A [%]
V1	235,0	253,3	11,5
V2	236,3	265,7	13,8
V3	224,0	259,0	13,3



EXTRUSION ALLOY DEVELOPMENT

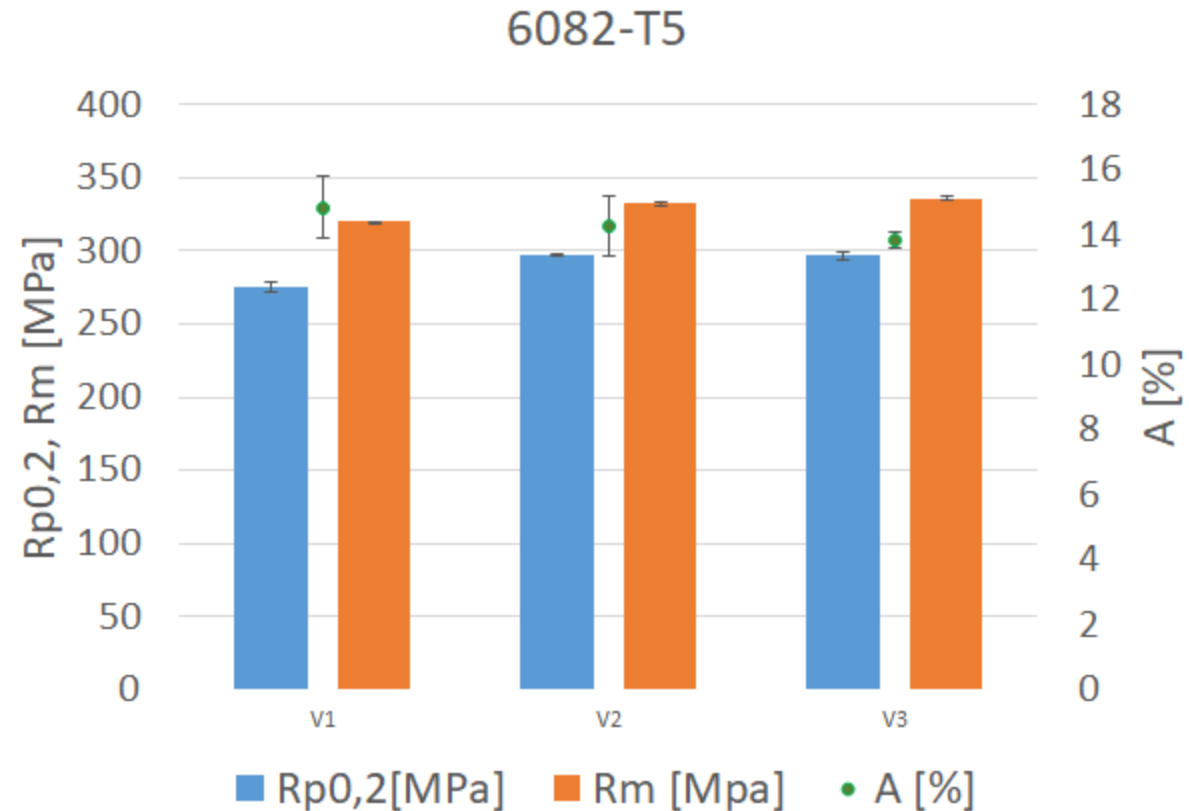
High scrap content 6082

6082	Si	Fe	Cu	Mn	Mg	Cr	Zn	Ti
Variant 1	0.939	0.223	0.043	0.626	0.824	0.071	0.223	0.0450
Variant 2	0.933	0.214	0.105	0.623	0.812	0.068	0.214	0.0440
Variant 3	0.929	0.232	0.167	0.622	0.911	0.071	0.232	0.1440

Static tensile test: EN ISO 6892-1:2020-05

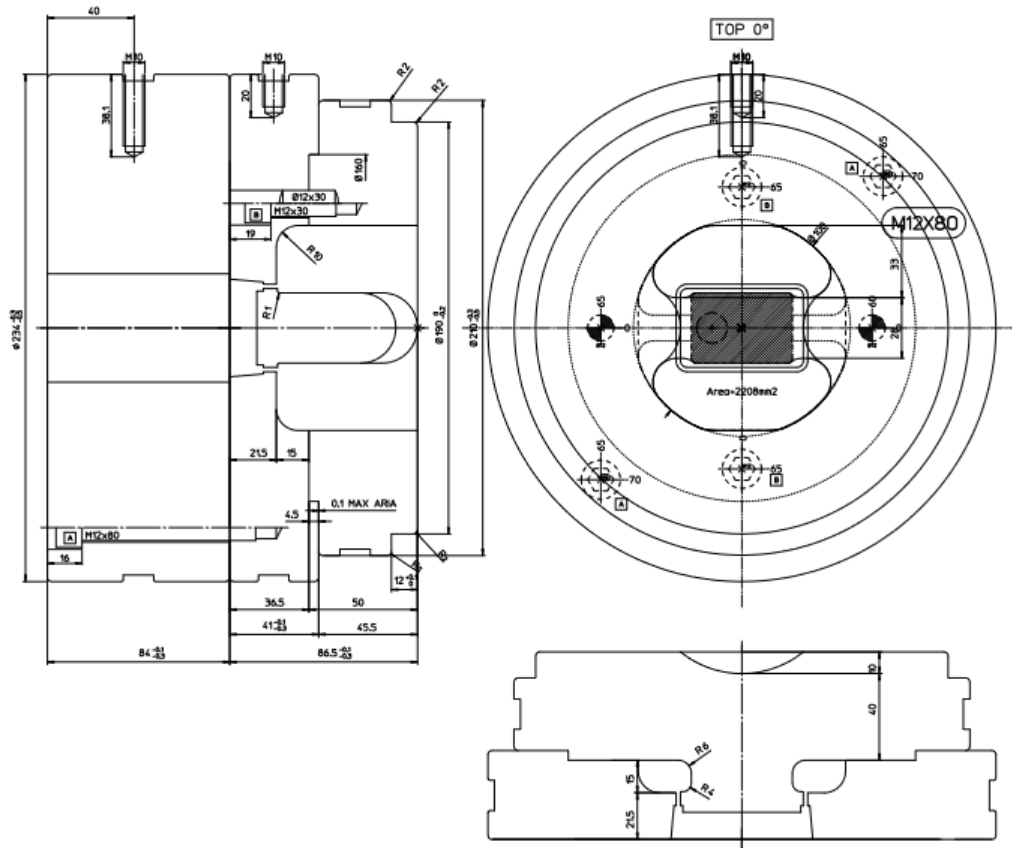
- Crosshead speed1 = 0,75mm/min
- croshead speed2 = 5mm/min.
- Gauge length 50mm

	Rp0,2 [MPa]	Rm [Mpa]	A [%]
V1	275,0	319,7	14,8
V2	297,0	332,0	14,3
V3	296,7	336,0	13,8

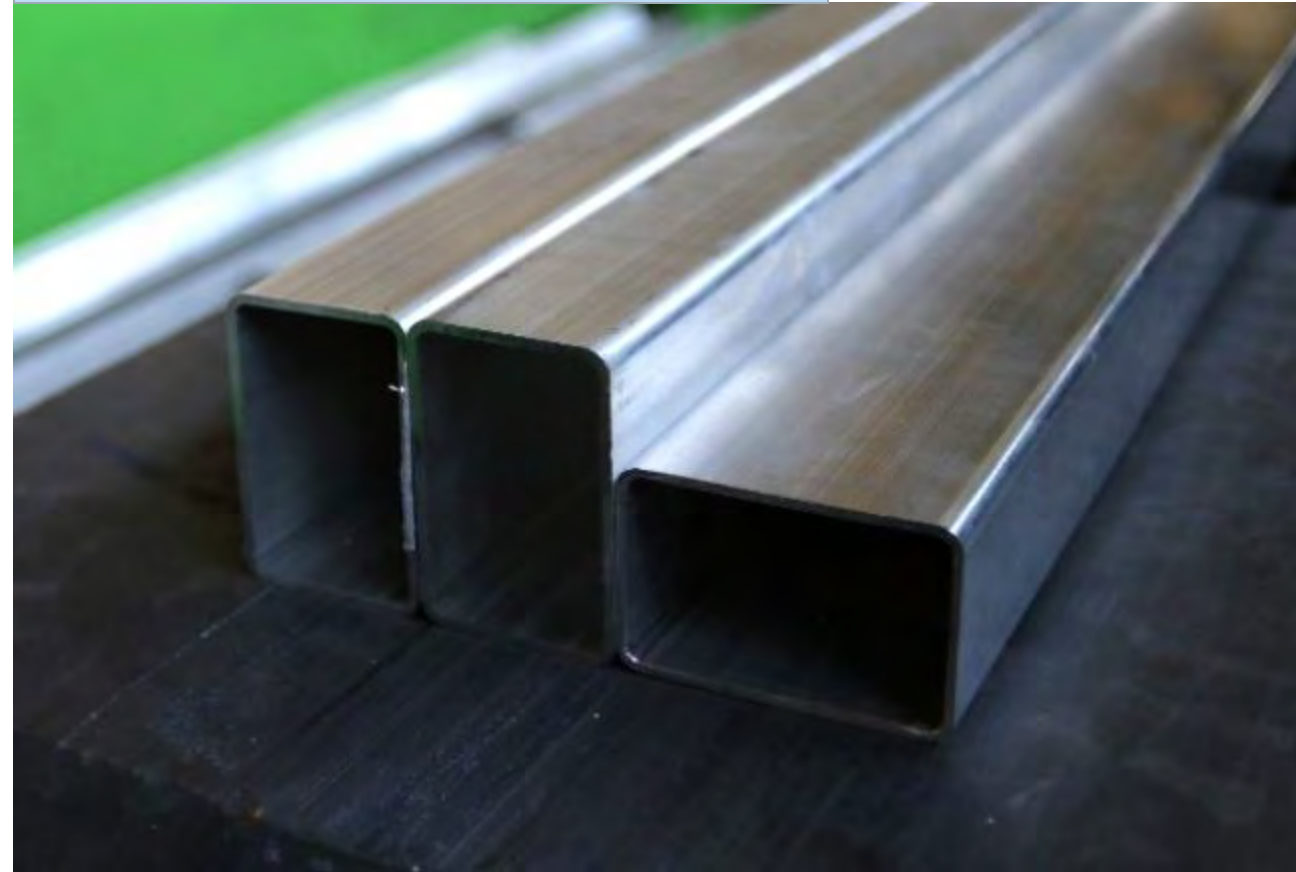


LABORATORY SCALE EXTRUSION DEMONSTRATOR

Die for 60x40x2mm hollow profile design



Hollow profiles from 3 SALEMA alloys



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.



BILLET CASTING

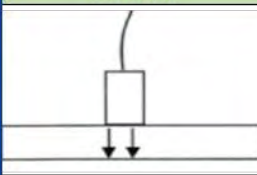
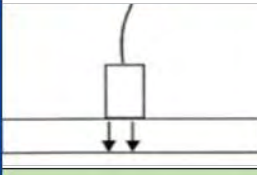
Casting Facility



SALEMA Billet



US Analysis

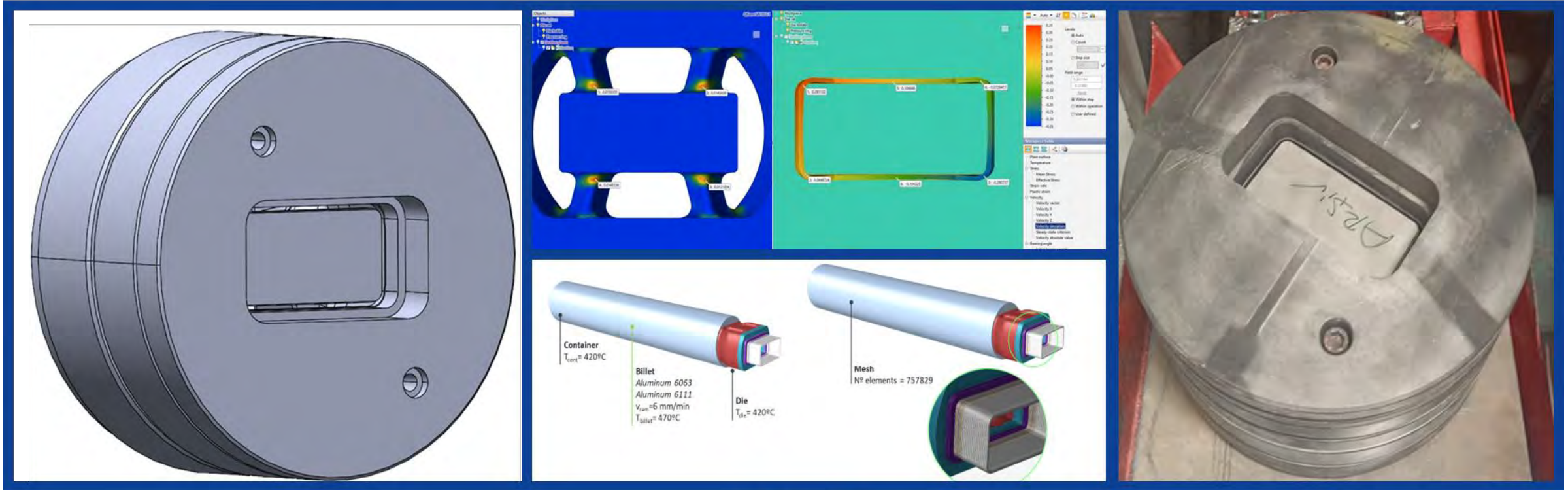
		Acceptance Criteria	Test Scope	Aging	
R&D6063	Length: 1200 mm Diameter: ø355mm	Aluminium	ASTM 594-9 Class A	100% Homogenization	
Test Sketch		Alloy	Total Billet Inspected		
		6063	1		
		Length and Direction			
				T- 360°	
RESULT					
ACCEPTABLE					
Heat No	Dimensions	Material	Acceptance Criteria	Test Scope	Aging
R&D6082	Length: 1700 mm Diameter: ø355mm	Aluminium	ASTM 594-9 Class A	100%	Homogenization
Test Sketch		Alloy	Total Billet Inspected		
		6082	1		
		Length and Direction			
					T- 360°
RESULT					
ACCEPTABLE					



DIE DESIGN

3D CAD MODEL

DIE MANUFACTURE



VIRTUAL

SIMULATION

PHYSICAL



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.

EXTRUSION

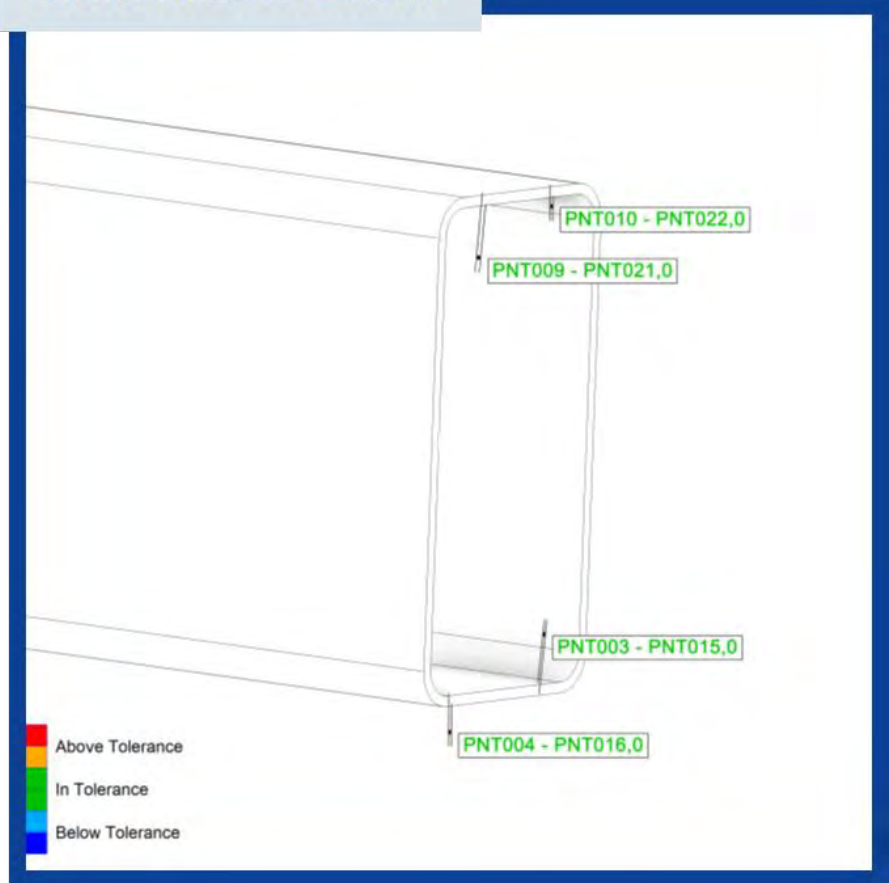
Extrusion Practices



SALEMA Profile



CMM Measurement



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.

CHARACTERIZATION AND TESTS CONDUCTED



BATTERY BOX						FRONTAL FRAME					
Test	Responsible	Amount	Profile No	Alloy	Standard	Test	Responsible	Amount	Profile No	Alloy	Standard
Tensile Test	ASAS	3	20213	6063	EN ISO 6892-1:2020.	Tensile Test	ASAS	3	20240	6063	EN ISO 6892-1:2020.
Tensile Test	ASAS	3	20213	6082	EN ISO 6892-1:2020.	Tensile Test	ASAS	3	20240	6111	EN ISO 6892-1:2020.
Tensile Test	Eurecat	3	20213	6063	400 mm specimen profile	Tensile Test	IMN	3	20240	6063	400 mm specimen profile
Tensile Test	Eurecat	3	20213	6082	400 mm specimen profile	Tensile Test	IMN	3	20240	6111	400 mm specimen profile
OES Composition	ASAS	2	20213	6063		OES Composition	ASAS	2	20240	6063	
OES Composition	ASAS	2	20213	6082		OES Composition	ASAS	2	20240	6111	
EDS Composition	ASAS	1	20213	6063		EBS Composition	ASAS	1	20240	6063	
EDS Composition	ASAS	1	20213	6082		EBS Composition	ASAS	1	20240	6111	
Optic Microstructure	ASAS	1	20213	6063		Optic Microstructure	ASAS	1	20240	6063	
Optic Microstructure	ASAS	1	20213	6082		Optic Microstructure	ASAS	1	20240	6111	
SEM Microstructure	ASAS	1	20213	6063		SEM Microstructure	ASAS	1	20240	6063	
SEM Microstructure	ASAS	1	20213	6082		SEM Microstructure	ASAS	1	20240	6111	
Bake Paint	ASAS	1	20213	6063	EN ISO 6892-1:2020 at 180°C for 20 mins	Bake Paint	ASAS	1	20240	6063	EN ISO 6892-1:2020 at 180°C for 20 mins
Bake Paint	ASAS	1	20213	6082	EN ISO 6892-1:2020 at 180°C for 20 mins	Bake Paint	ASAS	1	20240	6111	EN ISO 6892-1:2020 at 180°C for 20 mins
3-Point Bending	ASAS	5	20213	6063	VDA 238 – 100	3-Point Bending	ASAS	5	20240	6063	VDA 238 – 100
3-Point Bending	ASAS	5	20213	6082	VDA 238 – 100	3-Point Bending	ASAS	5	20240	6111	VDA 238 – 100
Tensile Test - Aniso	ASAS	3	20213	6063	EN ISO 6892-1:2020.	Tensile Test - Aniso	ASAS	3	20240	6063	EN ISO 6892-1:2020.
Tensile Test - Aniso	ASAS	3	20213	6082	EN ISO 6892-1:2020.	Tensile Test - Aniso	ASAS	3	20240	6111	EN ISO 6892-1:2020.
EBS Composition	IMN	1	20213	6063	400 mm specimen profile for per alloy	OES Composition	IMN	2	20240	6063	400 mm specimen profile for per alloy
EBS Composition	IMN	1	20213	6082		OES Composition	IMN	2	20240	6111	
TEM Microstructure	IMN	1	20213	6063		EBS Composition	IMN	1	20240	6063	
TEM Microstructure	IMN	1	20213	6082		EBS Composition	IMN	1	20240	6111	
						Optic Microstructure	IMN	1	20240	6063	
						Optic Microstructure	IMN	1	20240	6111	
						TEM Microstructure	IMN	1	20240	6063	
						TEM Microstructure	IMN	1	20240	6111	

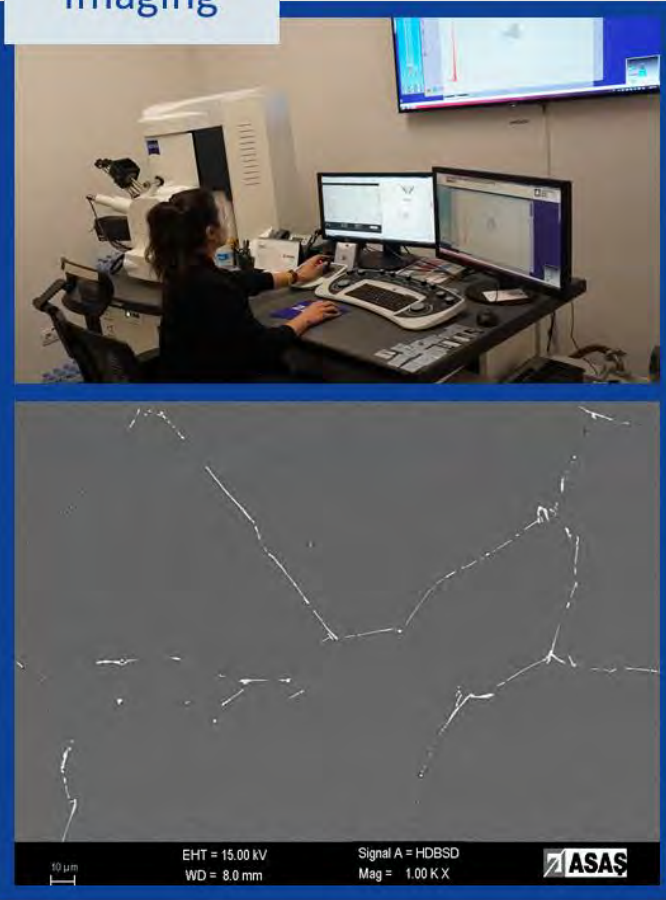


The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.



CHARACTERIZATION AND TESTS CONDUCTED

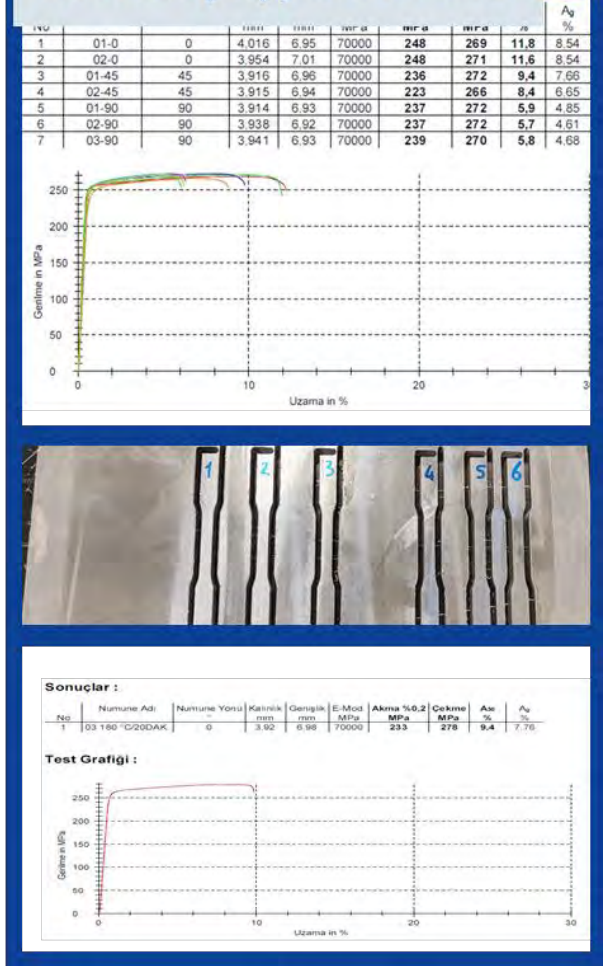
Imaging



Mechanical Tests



Anisotropy / Bake Paint



Bending



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.



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Summary

- Project introduction and video
- Scrap sorting system
- Development of HPDC SALEMA alloys
- Validation of HPDC SALEMA alloys in Shock Tower
- Alloy development and industrial validation in Hot Stamping
- Alloy development and industrial validation in extrusion
- Validation procedure of new alloys by an OEM



Validation procedure of new alloys by an OEM

- CRF - Stellantis contribution to demo development
- CRF activities on:
 - WP4 – High Pressure Die Casting (HPDC)
 - WP5 – Cold Stamping
 - WP6 – Extrusion
- Industrial validation in Cold Stamping
- Industrial validation in Frontal Frame
- Key Take-Aways



Fiat Research Center (CRF)



CRF CONTRIBUTION ON DEMONSTRATORS



- AUTOMOTIVE REQUIREMENTS ON STRUCTURAL COMPONENTS
 - Participated in the alloy development
 - Mechanical and Functional (weldability, corrosion, adhesion compatibility, etc.) properties
 - Internal and International standard
 - Standard alloys vs SALEMA alloys
 - Comparison based on real structural component requirement



CRF ACTIVITIES ON WP 4 – 5 – 6

• CORROSION RESISTANCE

- Provided mainly by Black E-Coat / Cataphoresis in automotive
 - ASTM B368 - Copper-Accelerated Acetic Acid-Salt Spray (Fog) (CASS test)
 - Cataphoresis compatibility
- Weight loss differential between variants and alloys
 - ASTM G85:A3 - acidified synthetic sea water testing (SWAAT test)



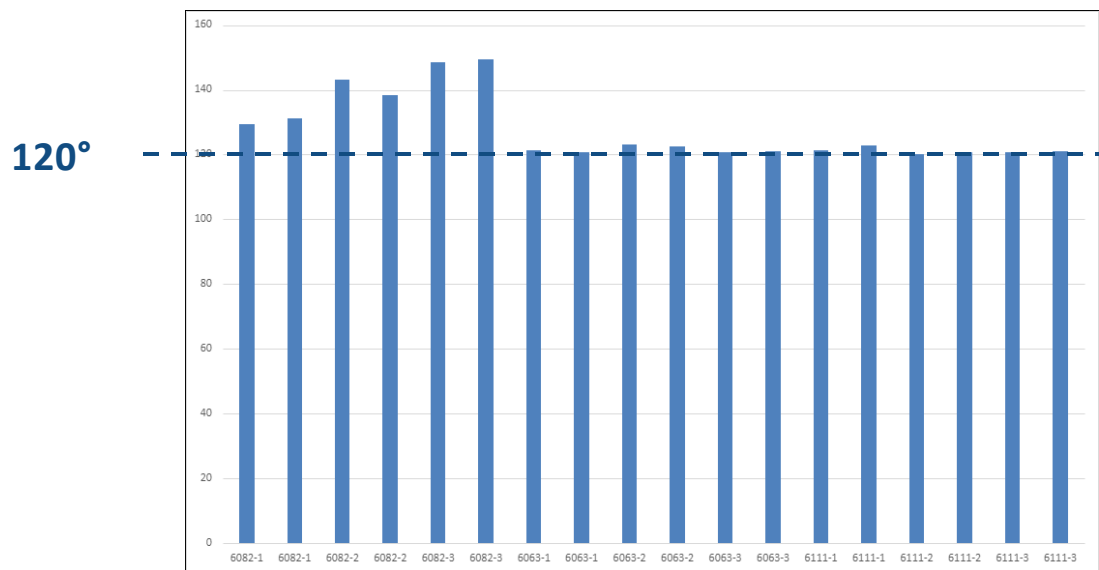
example:
HPDC – WP4

Alloy	Heat Treatment	Initial Weight	Weight after 168 h CASS	Weight loss	
				(g)	%
V4	F	122.2	113.2	9.0	7.4
V6		119.6	109.0	10.6	8.8
V4	T6	120.5	119.3	1.2	1.0
V6		116.5	114.3	2.2	1.9

CRF ACTIVITIES ON WP 4 – 5 – 6

- BENDING CHARACTERIZATION

- Important in wrought alloys, few examples for casting alloys in OEM requirements
- Stamping and Extruded SALEMA alloys
- HPDC in samples and in final demo → good behavior towards F vs HT temper



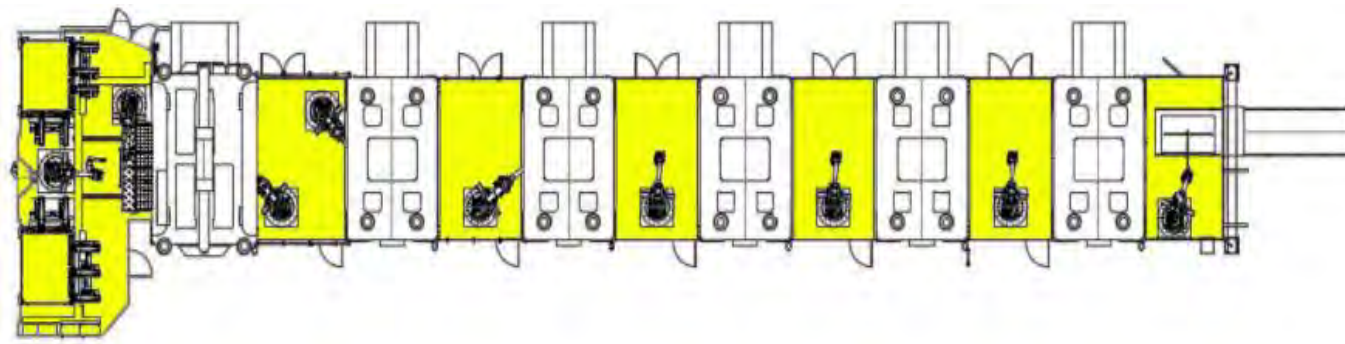
Alloy	Heat Treatment	Bending VDA 238-100	
		average	st.dv
V4	F	22.3	7.0
	T6	58.5	0.6
V6	F	23.1	9.9
	T6	51.4	1.9

INDUSTRIAL VALIDATION IN COLD STAMPING

• PROJECT TARGET

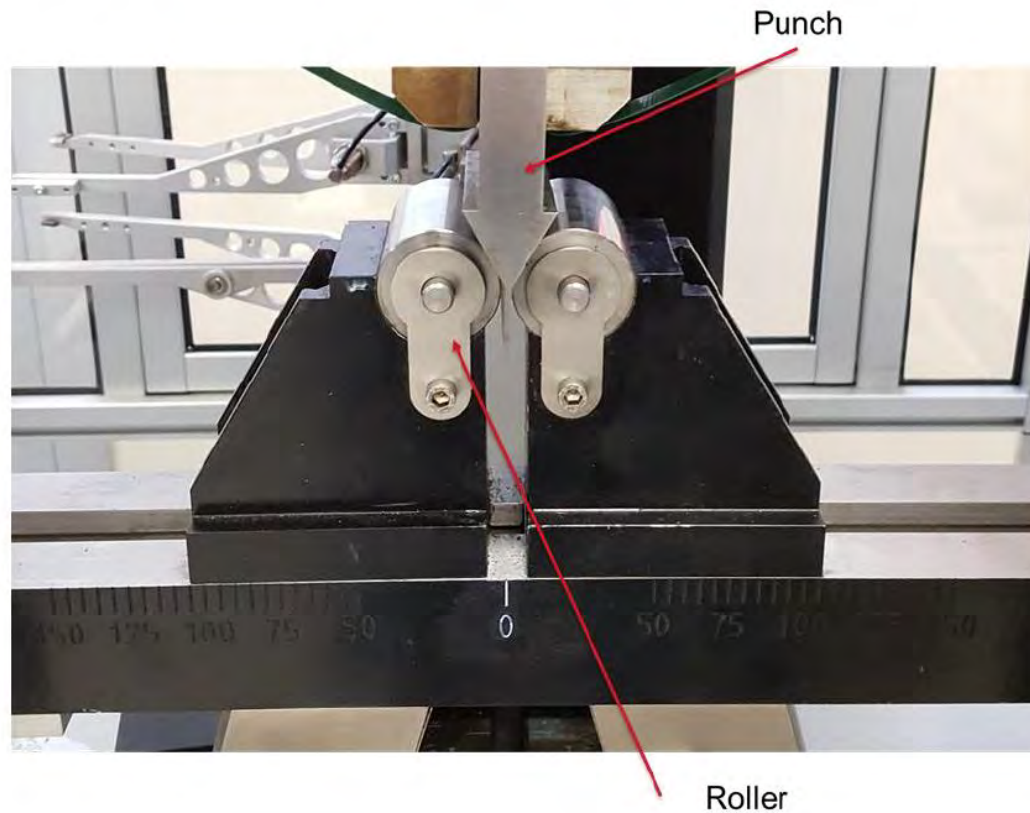
- Use of aluminum with high recycle content
 - 5754 H0 temper 70 - 85%
 - 6181A T4 temper 70 - 85%
- Inner hood demonstrator (Jeep Renegade)
- Thickness 0,9 mm
- Use the current assets in production for primary alloys

		Rp [MPa]	Rm [Mpa]	A [%]	Bending α [°]
5754	70%	97	210	22	110
5754	85%	100	212	22	
6181A	70%	163	276	24	110
6181A	85%	172	282	24	

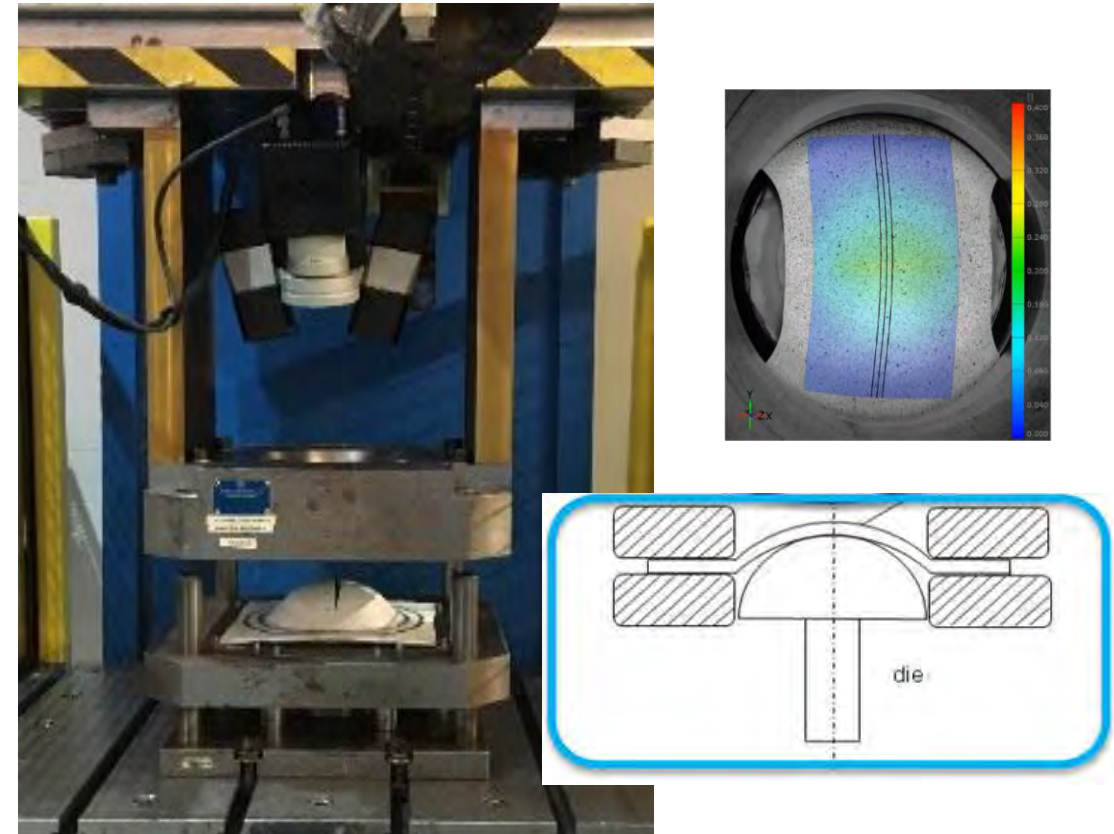


INDUSTRIAL VALIDATION IN COLD STAMPING

- BENDABILITY VDA 238-100



- COLD FORMING: FLD



- CORROSION RESISTANCE

- ASTM G85:A3 (SWAAT)
weight loss differential



5754



6181A

- ASTM B368 (CASS)
cataphoresis compatibility



5754

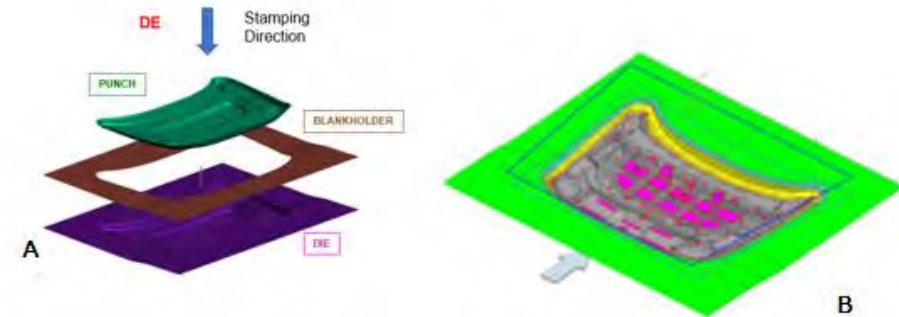


6181A

INDUSTRIAL VALIDATION IN COLD STAMPING

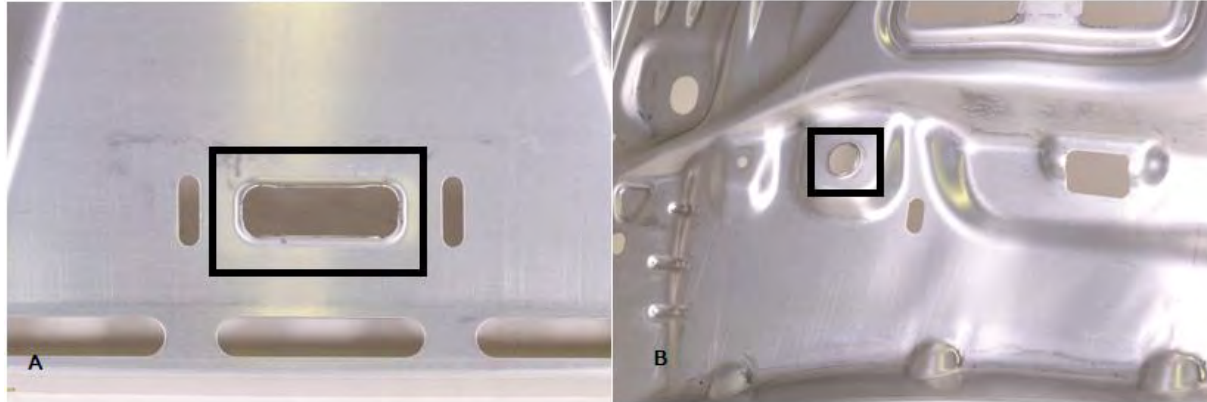
- DEMONSTRATOR MANUFACTURING

- Mirafiori Press Shop, Mirafiori Plant, Turin, ITALY



INDUSTRIAL VALIDATION IN COLD STAMPING

- QUALITY ASSESSMENT

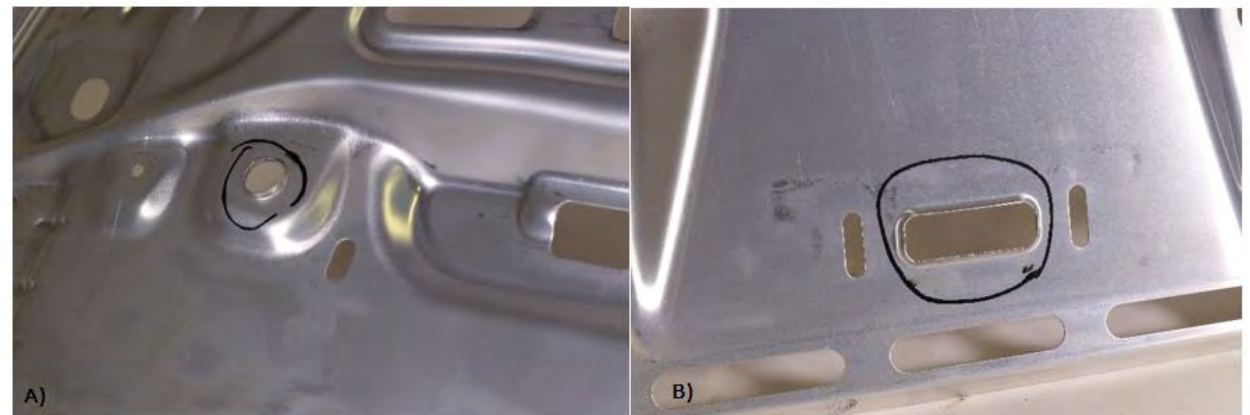


 **5754**

No cracks in maximum deformation zones (holes)
Keeps performance regardless high recycled content
OK for current production

6181A 

Cracks on most deformed zones
Show sensitivity to high recycle content
Need some design tuning for current production

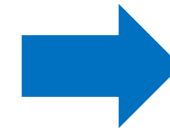


INDUSTRIAL VALIDATION IN FRONTAL FRAME

- Demonstrator Development

- **FROM:** Low Pressure Die Casting (LPDC) in Maserati MC20
- **TO:** High Pressure Die Casting (HPDC) for segment C-D car
- Main advantages: - high volume production
- cost reduction thanks near net shape features
- Mechanical requirements:

Rp [MPa]	Rm [Mpa]	A [%]
180	230	10



INDUSTRIAL VALIDATION IN FRONTAL FRAME



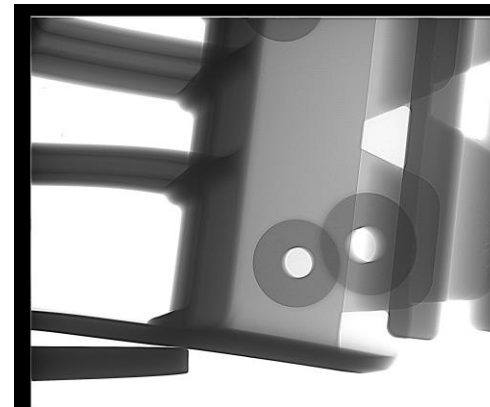
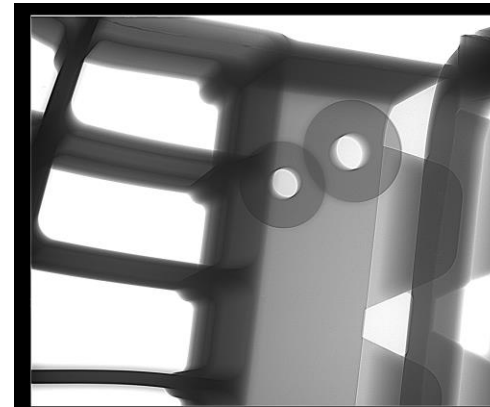
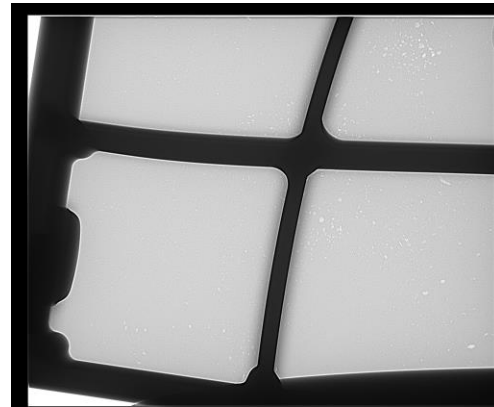
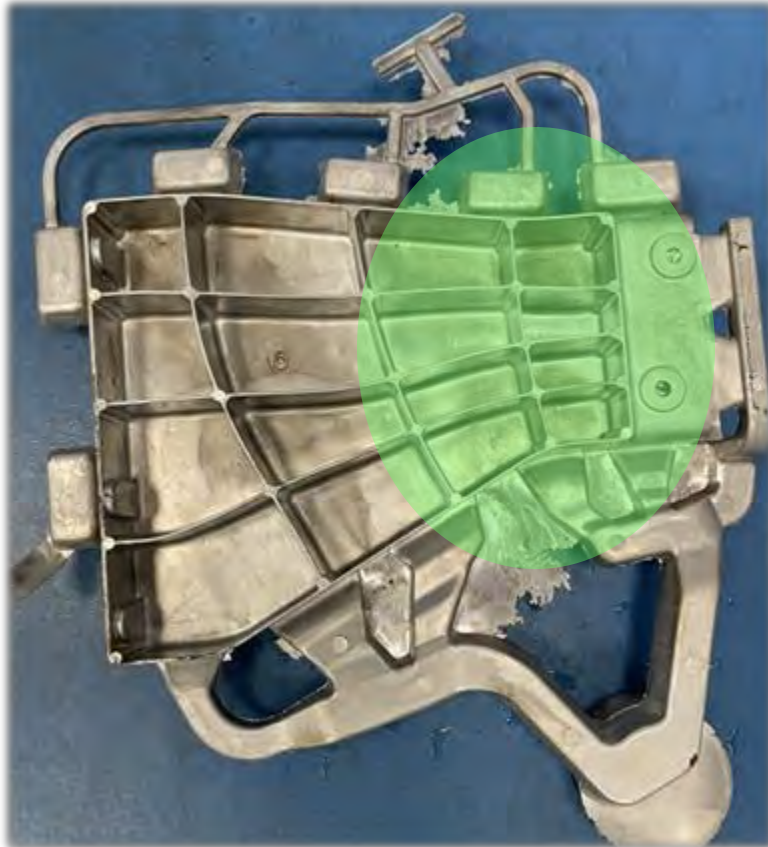
- PRODUCTION IN ENDURANCE S.P.A

VIDEO



INDUSTRIAL VALIDATION IN FRONTAL FRAME

X-RAY MAPPING COMPLETED



Very sound area



The project has received funding from the European Union's Horizon 2020 research and innovation programme under grant agreement No 101003785.

INDUSTRIAL VALIDATION IN FRONTAL FRAME



- MECHANICAL CHARACTERIZATION

- TENSILE
- FATIGUE
- TOUGHNESS
- X-RAY
- **MICROSTRUCTURE**
- **BENDING**
- **HETEROGENEOUS WELDING WITH SHEETS ALLOYS**

Eurecat
&
University of Padova

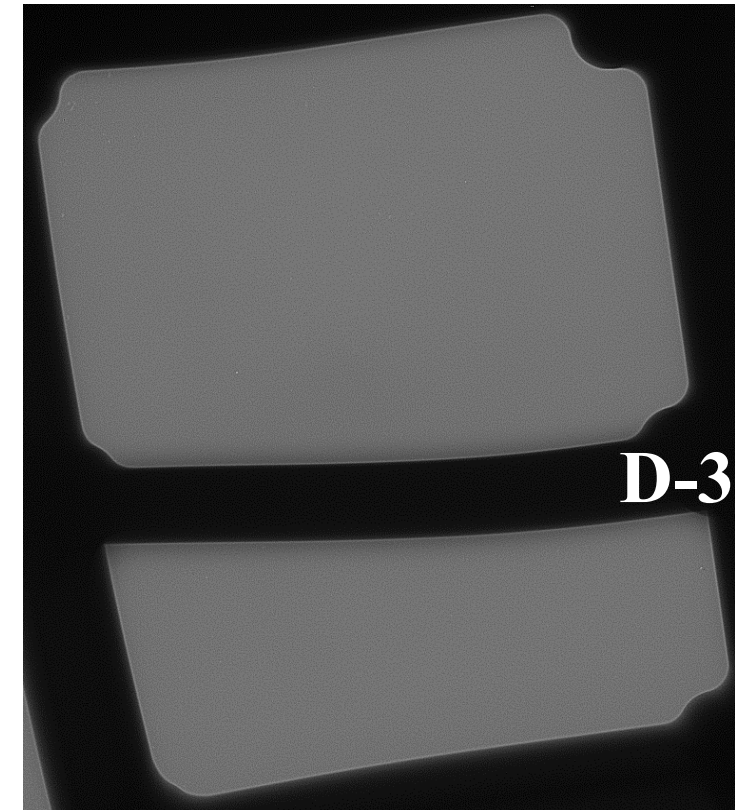
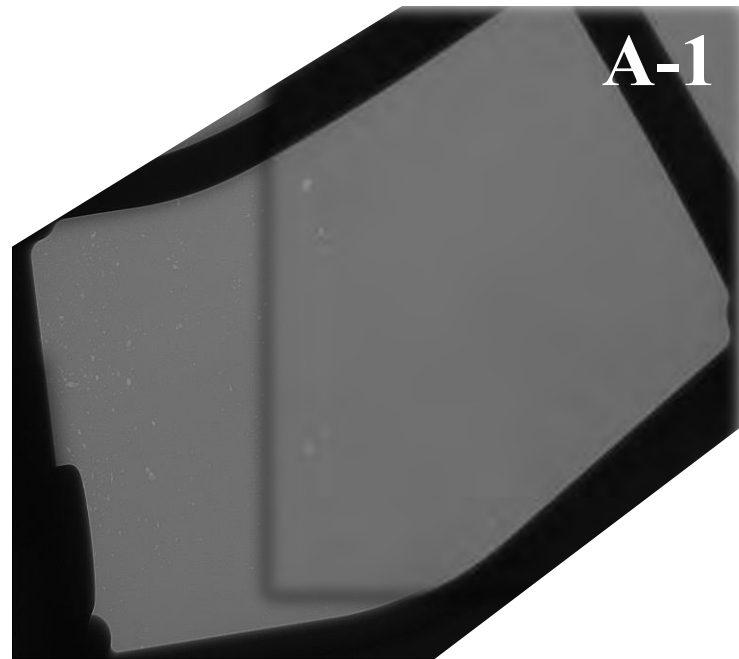
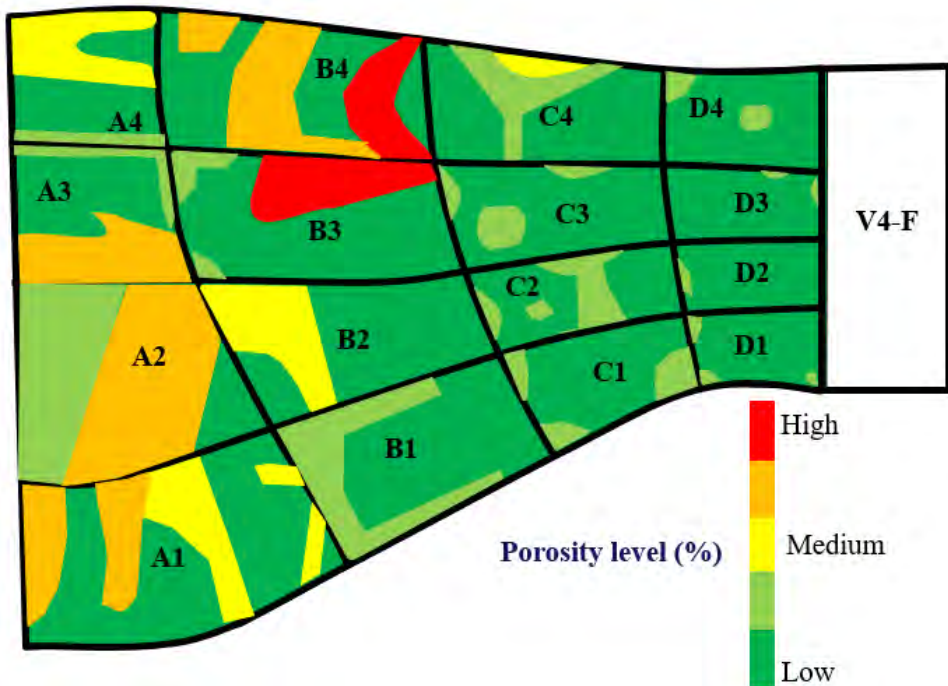


	angle [°]	st.dv
As Cast	25,1	7,5
T5	13,2	9,2
T6	54,4	3,7



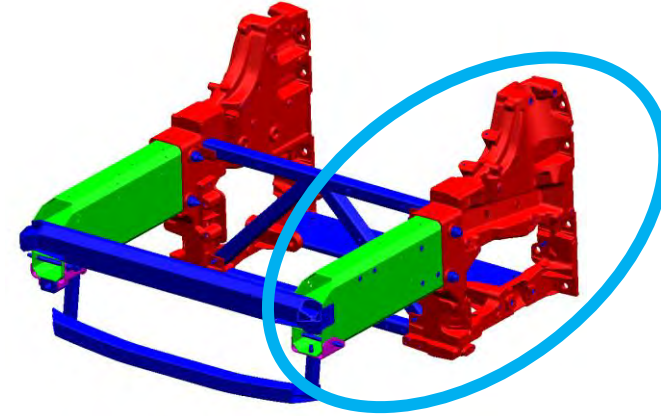
INDUSTRIAL VALIDATION IN FRONTAL FRAME

- X-RAY ANALYSIS (University of Padova, Osama Asghar – Franco Bonollo)



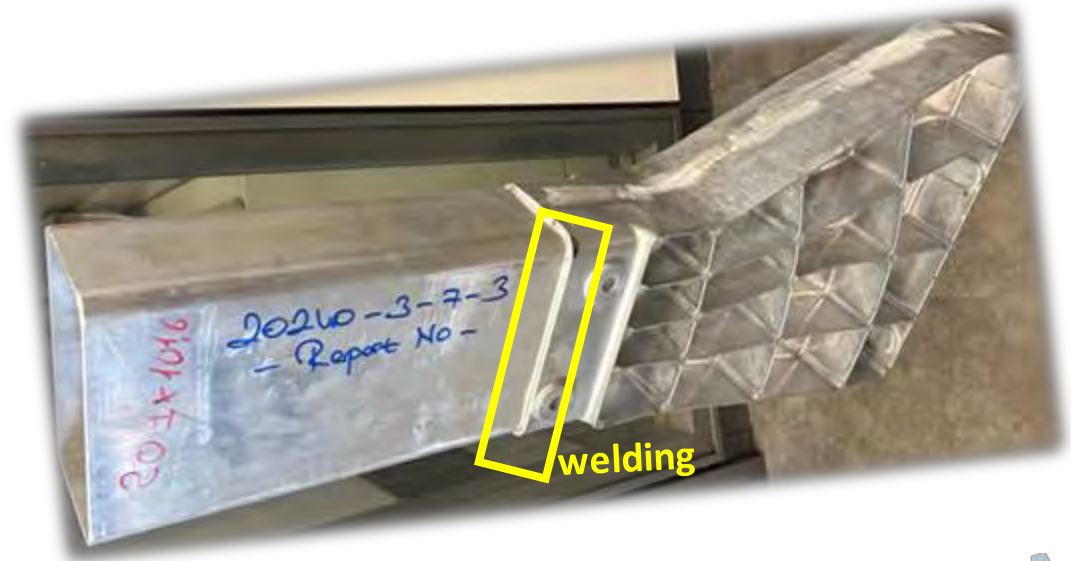
INDUSTRIAL VALIDATION IN FRONTAL FRAME

- FINAL ASSEMBLY HPDC – EXTRUDED



- WELDING VALIDATION

- Micrographic inspection
- Tensile test on welding bead
- Non-Destructive Testing



INDUSTRIAL VALIDATION IN FRONTAL FRAME



- KEY TAKE-AWAYS:
 - Alloy is suitable for structural components
 - No major differences compared to primary alloys in manufacturing
 - Design tuning needed for improving crash behavior
 - Crash test missing before complete industrialization
- FURTHER DEVELOPMENT OF DEMONSTRATOR – EU project
 - **FLEXCRASH** – Improve strength and crash behavior with hybrid AM
 - **RESTORE** – Remanufacturing with hybrid for another vehicle segment





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